PROGRESS REPORT GROUND WATER REMEDIATION SYSTEM SECO PRODUCTS FACILITY WASHINGTON, MISSOURI

March 5, 1991

Prepared for

Hussmann Corporation 12999 St. Charles Rock Road Bridgeton, MO 63044

Prepared by

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Geraghty & Miller, Inc., appreciates the opportunity to work for Hussmann Corporation at the SECO Products facility. If you have any questions or comments concerning this report, please contact one of the individuals listed below.

Respectfully submitted,

GERAGHTY & MILLER, INC.

Gregory D. Sengelmann

Project Scientist I

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Memorandum

Subject: SECO Groundwater Assessment

From: Leslie Jennemann

Geologist, RCRA/GEOL

Thru: Bill Pedicino

Chief, RCRA/GEOL

To: Dave Doyle

Chief, RCRA/GEOL

Re: Review of Progress Report

I have reviewed the document entitled "Progress Report: Ground Water Remeditation System SECO Products Facility Washington, Missouri". I have also reviewed the "Phase II Ground Water Assessment and Remediation System" report, the "Remedial Investigation Report, progress reports, and the file in general. I concur with the determination made by Harry Gabbert in the December 6,1991 memo to you on the Phase II report, that SECO is not in compliance with the 3008(h) Order. In addition to Harry's comments, the following are provided with respect to the groundwater monitoring system in general and the submittal under consideration.

Does the facility have a NPDES permit for the parameters in the groundwater remediation system effluent? In particular, 1,2-DCE?

General

Well Construction

SECO has not provided an adequate characterization of the upper most aquifer, nor has it made an adequate determination of the rate and extent of contamination in relation to background levels as required by the 3008(h) AOC.

The facility must provide a series of isoconcentration maps which depict the movement of the contaminant plume such as the one provided in this report (Diagrams 1 and 2) as an example. These maps must be based on representative and discrete groundwater samples; and the data must have been validated (QA/QC check).

The monitoring well system does not provide adequate control in terms of both the horizontal and vertical extent of contamination.

The design and installation of certain wells in the monitoring well system are inadequate in terms of yielding representative samples; in other wells a determination can not be made.

A full review of the monitoring well system is warranted. The condition of the well pad, inner and outer casings, cap, etc. must be noted. All wells must be checked for siltation, if over

15% occluded, the well must be redeveloped.

The monitoring well system must yield representative samples.

The individual wells must be screened in an appropriate interval, and the screen must be an appropriate length. In the EPA TEGD (OSWER-9950.1), it is stated that "When a single well cannot adequately intercept and monitor the vertical extent of a potential pathway of contaminant migration at each sampling location, the owner/operator should have installed a well cluster.". When an aquifer or preferential pathway to be monitored is greater than 10-15 feet, it is necessary to emplace a cluster of wells. The well screen should be no greater than 15 feet, and 10 feet is strongly suggested.

EPA requests that any grain size analyses used to determine the appropriate screen slot size and filter pack used in the well construction for each series of wells be referenced or submitted. If no grain size analyses were used, explain how the slot/filter pack sizes were determined.

Except for MW-1 through MW-6, all the wells were constructed as composite wells using PVC casing and stainless steel screens. Explain the exact method by which the casing and screen was joined. Was a thread connector used to join the PVC and steel? PVC Also state the type or grade of stainless steel used.

A statement regarding the rationale for use of PVC casing and screen must be made. The facility must address the possible sorbing of chemical constituents into the PVC in terms of the chemicals present in the site groundwater. The use of PVC eliminates the future argument that the chemical constituents which may have be sorbed into the PVC, are desorbing back into the well water sampled thus creating higher levels of contamination.

The method of emplacing the bentonite seal is needed, ie. were the bentonite pellets slurried then tremied down the hole? If not, were there any problems with bridging in the seal? Explain, or reference the whereabouts of this information.

It is strongly reccommended that a continuous soil sample be observed by the field geologist. Future well constructions should have continuous well samples logged.

In addition to the aforementioned requirements, the following comments are provided for the individual well series:

MW-series

Placement

No upgradient middle sand wells are present which may be used as a background well. It is necessary to install a background well

in the middle sand. 6

Construction

Design and installation records for MW-1 through 5 were reviewed by Reed and Asc. in the RAP. The conclusion reached by Reed was that the system was adequate for indicating water quality, EPA suspects that this is not the case. EPA cites the Monitoring Well Installation, Sampling and Analysis report from February, 1983. It is stated that wells are constructed of PVC, have 15 foot screens lengths, a .006 inch slot size was used, and "Coarse filter sand was used as backfill material around the well screens". It is further stated in reference to well development, that "no reasonable amount of activity would achieve clear water." It was stated that the wells were developed using a hand bailer which may have been insufficient for good development. have these wells been redeveloped? It has been noted that MW-1 and MW-3 have been dry during a sampling round.

SS-series

Placement

It is important to note that the SS wells were dry during January and February. I sthis due to the water table being lower than the well screen, or a problem with the well?

SS-1 is the furthest downgradient shallow well; however, no chemical data was presented for this well. SS-2 shows high levels of TCE and t-1,2-DCE in recent samplings. SS-3 has only two sampling events associated with it. Explain why no data is present for SS-1, and little is present for SS-3. Additional monitoring wells are necessary in the shallow sand downgradient from MW-5 and RW-2 to ascertain the horizontal extent of contamination near to Dubois Creek.

Isoconcentration maps can not be constructed with 2 data points, therefore, the facility must wait to construct these until more shallow wells are installed.

Construction

The well construction records for the shallow well series SS-1 through SS-3 were reviewed. Specific details of the well completion and development were not found, and must be included or referenced.

MS-series

Placement

No upgradient well exists for the middle sand; an upgradient well

must be installed. No downgradient well monitoring the middle sand exclusively is present, and must be installed to the east and northeast of MW-5 and RW-2. Replacement wells for MS-1, MS-2 and MS-5 are needed due to the overlong screen lengths of those wells. An additional well is needed to the east of RW-4/RW-5, and another may be needed on the other side of Dubois Creek.

Construction

Construction records for middle aquifer wells, MS-1 through MS-6 were reviewed. The screened interval for MS-2 and MS-5 were 35 /5 feet, and that of MS-2 was 20 feet. The well logs for these wells indicate a variable lithology, changing from "gravelly sand" to "silty clay" in MS-2, and "silty sand" to "silty clay" within the screened interval of MS-5. Excessive dilution by the introduction of uncontaminated groundwaters into the preferred zone of contaminant movement will not yield the sampling of discrete portions of the aquifer. In some cases this may result in the contamination present in the groundwaterbeing below the detection limits of the laboratory. EPA believes that these wells should be replaced with ones that can sample from a discrete zone.

It is noted on Figure 5, that MS-4 has been abandoned. Explain the procedures used in abandonment, or reference the whereabouts of these procedures. Why was this well abandoned?

MD-series

Placement

MD-1 has shown measureable concentrations of DCE the last two sampling rounds. Due to the fact that the well screens in the MD series wells are 5 feet long, concern that the screen is occluded by sediment exists. The well maintenance inspection and subsequent actions reccommended above should be performed prior to any final judgement about these wells is made.

Construction

The logs for the deep well series were examined. Figure 5 shows that MD-3 has been abandoned. Why? Explain the procedures used in abandonment or reference the whereabouts of these procedures.

RW-series

Placement

It has been noted that RW-1 has been redeveloped due to a break in the screen. How was the break discovered? What percent occlusion had been found in the well prior to the decision to rework the well? Were the other wells checked; with what re-

sults?

A statement regarding the estimated capture zones (from Appendix E of Phase II report) accuracy and any modifications made after operating the system should be included. It appears that the estimated capture zones for RW-4 and RW-5 were not large enough to control migration to the east and to the south. Additionally, RW-6 was not installed due to the fact that RW-5 runs intermittently. How has the lower transmissivity affected the capture zones predicted? Are more recovery wells proposed at this time? It is strongly suggested that several more wells be considered, or another approach to containment/remediation be devised.

Construction

The well log of RW-1 was reviewed; the use of two well diameters and two screen sizes at different depths is not shown in the log. Explain, in detail the exact methods used to construct this well.

Provide the well logs for RW-2 through RW-5, or reference the whereabouts of this data. The majority was a support

Specific Comments

- 1. pg. 1, ¶2- Although the EPA letter stated that "...Hussman should begin work on the recovery sytem... ", it also stated that "it is EPA's position that the uppermost aquifer has not been defined as required by 40 CFR 265.90(a)".
- 2. pg. 2,¶1- Due to the fact that the RW-5 well has had such slow recovery times, it is assumed that the expected transmissivities were too great. The calculations used to derive the capture zone should be redone and submitted in the next report.
- 3. pg.2,¶2- The use of mud rotary drill rigs is not the best choice to drill monitoring wells due to contamination from the drilling mud. Was a contaminant free drilling mud used?
- 4. pg. 2,¶3- How long was the bentonite seal allowed to hydrate before well completion?
- 5. pg. 3,¶1- Has the permitted NPDES discharge shown any non-compliance episodes? When?
- 6. pg. 3,¶2- Why is MD-3 not considered in the quarterly sampling? According to the sampling data presented in Table 2., MD-1 has had significant increases in the last two sampling events. Again, EPA would like to ascertain the well screen is clear and that the MD wells are capable of yielding representative samples.
- 7. pg.4,¶2- Was the effluent sampled at the same discharge point as the NPDES discharge?

- 8. pg. 4,¶4- It would be usefule to present the flow rates and total gallons for each well in tabular form. See Table 3
- 9. pg.5,¶1- What caused the "break" in the well screen of RW-1, and how was it discovered?
- 10. $pg.6, \P1-$ Is data validation performed on the analytical results by a separate laboratory?
- 11. pg. 6, ¶2- What has caused the shallow sand wells to become dry? Decrease in water table? They have always been dry see Table?
- 12. pg. 6, ¶3- Has information regarding the flooding periods been recorded? When have these groundwater reversals occurred? A list of these dates and any water level information associated with them would be useful in determining the directional changes in flow at this site.
- 13. pg.7,¶1- The maps presented do not adequately evaluate the pump and treat system. Further examination of the system must be performed and modifications must be made due to the lower than anticipated permeabilities at RW-5. Perhaps the use of "pulsed pumping" (perhaps after interior wells have been installed) should be condsidered (if not already). This may allow residual NAPLs and sorbed contaminants to diffuse to zones of higher conductivity. Cycling of different pumping wells may also allow the remediation of stagnation zones.

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INTRODUCTION

This ground water remediation system progress report is being submitted to the United States Environmental Protection Agency (EPA) Region VII and the Missouri Department of Natural Resources (MDNR) on behalf of Hussmann Corporation. The ground water remediation system was installed at the SECO Products facility in Washington, Missouri, as a portion of the work required by a 3008(h) Consent Order signed by the EPA and Hussmann Corporation.

BACKGROUND

A Ground Water Quality Assessment Plan was submitted to EPA Region VII as part of Hussmann Corporation's Remedial Action Plan. The plan was subsequently approved by an EPA 3008(h) Consent Order. Geraghty & Miller, Inc. (G&M) conducted the ground water quality assessment at the SECO Products facility and submitted the results of that investigation in documents entitled "Progress Report, Ground Water Assessment, Phase II" dated April 12, 1989, and "Phase II Ground Water Assessment and Remediation System" dated June 21, 1989. The "Phase II Ground Water Assessment and Remediation System" document included a proposed sitewide ground water remediation system which was subsequently approved by the EPA. This system was started on January 29, 1990.

GROUND WATER RECOVERY SYSTEM INSTALLATION

Five ground water recovery wells (RW-1 through RW-5) were installed at the locations shown on the site map (Figure 1). Six recovery wells were initially proposed; however, it was determined during construction and development of recovery well RW-5

that installation of the sixth recovery well proposed near the southern edge of the site would not contribute to the overall effectiveness of the system because of the decreased saturated aquifer thickness and low transmissivity in this area. Recovery well RW-5, the southernmost recovery well, runs only intermittently and requires approximately 12 to 24 hours to recover after pumping the well dry.

The recovery wells were installed with a truck-mounted rig using mud rotary techniques. Cuttings were logged continuously and split spoon samples were collected at five-foot intervals and at lithologic breaks. The boreholes were drilled to the top of the clay layer below the middle sand aquifer. Each boring was logged by a G&M hydrogeologist using the Unified Soil Classification System. Boring logs are included in Appendix A.

The wells were constructed of six-inch-diameter Schedule 40 PVC casing and screen (0.018-inch slot). The screened interval was placed opposite the shallow and middle sand aquifers, and a WB-35 sand pack was emplaced in the annular space between the borehole and screen from the bottom of the borehole to approximately two feet above the top of the screened section. A two-foot bentonite pellet seal was placed above the sand pack, and the remaining annular space was grouted to the surface with a cement-bentonite slurry. The wells were completed approximately one foot below grade inside concrete vaults. Monitor well construction schematics are presented in Appendix A. Table 1 summarizes the well completion details of each recovery well and monitor well at the site. The top-of-casing elevations were surveyed to the nearest 0.01 foot above mean sea level.

The rig and all sampling and development equipment were steam cleaned prior to drilling and before installation of each well. Sampling equipment was cleaned between each sample interval with an Alconox wash and a deionized water rinse. After installation the wells were developed by pumping and surging until the development water was clear and free of drilling mud and silt.

Following development, submersible pumps and water level sensors were installed in the wells, and an air-tight sanitary well head seal was fitted over the top of each well. A flow totalizer, pressure gauge, flow valve, and sample port were connected to the discharge piping at the well head (Figure 2). PVC discharge piping connecting the wells to the air stripper tower was installed and buried approximately three feet below ground level (BGL) (Figure 3). A blower capable of maintaining an air/water ratio of 100:1 or greater to optimize mass transfer of organics from the fluid phase to the vapor phase was connected to the bottom of the air stripper tower. The treated water is discharged from the air stripper tower to a drainage ditch that flows into Dubois Creek. A schematic diagram of the air stripper is shown on Figure 4.

SAMPLING AND ANALYSIS

As stipulated in the ground water recovery plan, the recovery wells and shallow and middle sand aquifer wells (except the six RCRA wells) will be sampled quarterly for the first year and semiannually thereafter until termination of the program. The deep sand aquifer wells (MD-1 and MD-2) will be sampled quarterly for the first year to confirm the absence of volatile organic compounds (VOCs) in the deep aquifer at the site. When the analytical results for one year confirm the deep sand aquifer is free of VOCs, the deep sand aquifer wells will be plugged and abandoned to prevent any chance of future cross contamination between the deep and middle and/or shallow sand aquifers.

The ground water samples will be analyzed for VOCs using EPA Method 8240. Ground water levels will be measured in all wells during each sampling round. The effluent from the ground water treatment system is being sampled in accordance with the requirements of the National Pollutant Discharge Elimination System permit. Table 2 summarizes the results of the sample analyses for the first year of operation for

each of the recovery wells; the shallow, middle, and deep sand aquifer wells; and the air stripper effluent stream. Table 3 summarizes the water level data collected since startup of the ground water recovery system for the recovery wells; the shallow, middle, and deep sand aquifer wells; and Dubois Creek.

In order to determine the treatment efficiency of the ground water recovery system, air stripper influent and effluent samples were collected during the first sampling round. The results of these analyses and the calculated removal efficiency of the air stripper are shown in Table 4.

OPERATION AND MAINTENANCE

Operation and maintenance procedures for the ground water recovery system are conducted according to the Operation and Maintenance Procedures Manual presented as Appendix B. Flow rate, total gallons discharged, water pressure, and condition of the tower and blower system are recorded daily on the Treatment Unit Inspection Log by SECO Products personnel (Appendix C). Any system failures or shutdowns because of inclement weather also are noted on the inspection log. System failures or shutdowns are reported to representatives of Hussmann Corporation and G&M within 24 hours.

Recovery well and monitor well inspections are performed by G&M representatives during each sampling round. Water level measurements, flow rates, total gallons discharged from each well, and water pressure are recorded on the Monitor/Recovery Well Data forms (Appendix D).

Any repairs or modifications made to the air stripper system, monitor wells, or recovery wells are recorded in a cloth-bound field notebook. Repairs to the ground water recovery system during the period from January 29 to December 31, 1990, are listed below.

Date	Repair
01/31/90	Reset amperage sensitivity to avert pump failure from power surges.
03/01/90	Clean out flow meter on recovery well RW-1.
03/13/90	Clean out flow meter on recovery well RW-1.
04/03/90 - 06/08/90	Recovery well RW-1 shut down because of sand entering well through break in screened section. Workover performed and well placed back on line.
04/12/90	New flow meter installed on recovery well RW-2.
05/17/90 - 05/30/90	Recovery system shut down because of Dubois Creek flooding.
08/01/90 - 09/19/90	Recovery system shut down for routine maintenance on air stripper tower. Cleaned out packing material and replaced with new packing.

The workover for recovery well RW-1 was conducted under the supervision of a G&M hydrogeologist. A truck-mounted mud rotary drilling rig was used to circulate the sand and silt out of the well and pull the submersible pump. The sand and silt material was flushed out of the well to a depth of 36 feet BGL. A four-inch-diameter flush-threaded PVC screen section (0.018-inch slot) was installed inside the original six-inch-diameter casing, and the annular space between the two casings was sand packed with a WB-35 water-washed sand. Following recompletion, the well was developed by surging and bailing until the development water was clear and free of silt. The submersible pump and water level sensors were reinstalled in the well, and the well was put back on line on June 6, 1990. A diagram of the recompleted well is presented in Appendix A.

REPORTING

Laboratory results are submitted to the EPA and MDNR within 45 days of receipt from the laboratory. An annual report summarizing the analytical results and water level data for the previous year will be submitted to the EPA and MDNR. The performance of the recovery well system will be reviewed, and any problems experienced with the system will be discussed in this report.

RECOVERY WELL SYSTEM EVALUATION

The ground water recovery system was placed in operation on January 29, 1990. The system is designed both to remove VOCs from the ground water and provide an effective hydraulic barrier prohibiting the downgradient migration of ground water containing VOCs. The recovery wells are screened across both the shallow and middle sand aquifers, although the shallow sand zone has been intermittently dry since water level monitoring of the discrete shallow sand aquifer wells was initiated.

Prior to starting the system, static water level measurements were collected from each well on-site, and a static water table map of the middle sand aquifer was constructed (Figure 5). The static water table map provides a basis for which to assess the amount of subsequent drawdown. This map indicates an east-west trending ground water divide exists at the site. The flow direction to the north of this divide is northerly toward Dubois Creek, while the flow direction to the south of this divide is to the southwest, also toward the creek. Historical water level data indicate a considerable range of water level fluctuations occurs in the shallow and middle sand aquifers. Annual variations can be as much as ten feet from high to low levels. The water levels in the middle and shallow zones appear, in large part, to be controlled by water levels in the Dubois Creek/Missouri River drainage system. Dubois Creek is generally the discharge area for these zones, although temporary ground water flow reversals occur during large-scale flooding events (Figure 6).



Figures 7, 8, 9, and 10 show the water table at the site after startup of the recovery system for the first through fourth quarters of 1990, respectively. These maps indicate the direction of ground water flow across virtually the entire site is now to the northwest toward the recovery wells. The ground water sink created by the recovery wells appears to be effectively capturing VOC-impacted water at the site.

Well No.	Well Diameter (inches)	Borehole Diameter (inches)	Well Material	Screened Interval (ft BGL)	Sand Pack (ft BGL)	Cement/ Bentonite Seal (ft BGL)	Top of Casing Elevation (ft MSL)
RW-1	6	9	PVC Casing PVC Screen (0.018" slot)	10-50	8-55	0-8	482.93
	4		PVC Screen (0.020" slot)	15.5-35.5 20	0-36		483.09
RW-2	6	9 7/8	PVC Casing PVC Screen (0.018" slot)	15-75	10-76	0-10	479.14
RW-3	, 6	9 7/8	PVC Casing PVC Screen (0.018" slot)	17-67 50	12-69	0-12	478.90
RW-4	6	9 7/8	PVC Casing PVC Screen (0.018" slot)	13-43 30	10-45	0-10	483.84
RW-5	6	9 7/8	PVC Casing PVC Screen (0.018" slot)	13-48 45	10-48	0-10	486.84
SS-1	2	9	PVC Casing SS Screen (0.018" slot)	10-15 5	8-15	0-8	483.22
SS-2	2	9	PVC Casing SS Screen (0.018" slot)	10-20 /	8-20	0-8	483.88

SS Stainless steel
BGL Below ground level
MSL Mean sea level

Well No.	Well Diameter (inches)	Borehole Diameter (inches)	Well Material	Screened Interval (ft BGL)	Sand Pack (ft BGL)	Cement/ Bentonite Seal (ft BGL)	Top of Casing Elevation (ft MSL)
SS-3	2	9	PVC Casing SS Screen (0.018" slot)	15-20 5	13-21	0-13	492.14
MS-1	2	9	PVC Casing SS Screen (0.018" slot)	26-41 \$5	24-43	0-24	482.32
MS-2	2	9	PVC Casing SS Screen (0.018" slot)	25-45 <i>20</i>	21-46	0-21	482.75
MS-3	2	9	PVC Casing SS Screen (0.018" slot)	34-44 10	29-50	0-29	491.77
MS-5	2	9	PVC Casing SS Screen (0.018" slot)	24.5-39.5	22.5-40	0-22.5	491.95
MS-6	2	9	PVC Casing SS Screen (0.018" slot)	34-39 5	32.5-47	0-32,5	492.15
MD-1	2	9	PVC Casing SS Screen (0.018" slot)	83-88	78-89	0-78	482.62

SS Stainless steel
BGL Below ground level
MSL Mean sea level

Well No.	Well Diameter (inches)	Borehole Diameter (inches)	Well Material	Screened Interval (ft BGL)	Sand Pack (ft BGL)	Cement/ Bentonite Seal (ft BGL)	Top of Casing Elevation (ft MSL)
MD-2	2	9	PVC Casing SS Screen (0.018" slot)	83-88 ≤	78-89	0-78	482.58
MW-1	2.5	6	PVC Casing PVC Screen (0.006" slot)	8.3-23.3 15	8-23.5	0-8	482.02
MW-2	2.5	6	PVC Casing PVC Screen (0.006" slot)	17.9-32.9	16.5-33	0-16.5	492.43
MW-3	2.5	6	PVC Casing PVC Screen (0.006" slot)	7.5-22.5	6-23.5	0-6	482.81
MW-4	2.5	6	PVC Casing PVC Screen (0.006" slot)	7.5-22.5 /5	6-22.5	0-6	481.83
MW-5	2.5	6	PVC Casing PVC Screen (0.006" slot)	11.8-26.8	10-29	0-10	484.24
MW-6	2.5	6	PVC Casing PVC Screen (0.006" slot)	23.4-38.4 /5	14-38.5	0-14	493.37

SS Stainless steel
BGL Below ground level
MSL Mean sea level

Well	Sample Collection Date	Laboratory	Laboratory Report Number	TOC (μg/L)	Toluene (µg/L)	1,1-DCE (µg/L)	t-1,2- DCE (µg/L)	1,1,1- TCA (µg/L)	TCE (µg/L)	Vinyl Chloride (µg/L)	1,2-DCA (µg/L)	Silver (µg/L)	рН
RW-1	12/05/88	NET	38640	0.0	-1.0	1.0	41.10	-1.0	49.40	-20.0	-1.0	0.0	0.00
	01/31/90	EMS	A200234	0.0	-50.0	-50.0	3000.00	-50.0	90.00	130.0	-50.0	0.0	0.00
	07/20/90	EMS	A210734	0.0	-5.0	6.0	9600.00	-5.0	700.00	-10.0	-5.0	0.0	0.00
	09/26/90	EMS	A214778	0.0	35.0	-5.0	2700.00	-5.0	5.80	28.0	-5.0	0.0	0.00
	10/15/90	EMS	A216233	0.0	-5.0	-5.0	3300.00	-5.0	88.00	77.0	-5.0	0.0	0.00
RW-2	01/31/90	EMS	A200236	0.0	-5.0	24.0	11000.00	-5.0	200.00	110.0	-5.0	0.0	0.00
	04/03/90	EMS	A204066	0.0	-5.0	11.0	11000.00	-5.0	440.00	110.0	-5.0	0.0	0.00
	07/20/90	EMS	A210735	0.0	-5.0	14.0	6500.00	-5.0	740.00	170.0	-5.0	0.0	0.00
	10/15/90	EMS	A216231	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	01/24/91*	EMS	A222561	0.0	-5.0	7.0	4,600.00	-5.0	600.00	130.00	-5.0	0.0	0.00
RW-3	01/31/90	EMS	A200237	0.0	-50.0	-50.0	2800.00	-50.0	55.00	55.0	-50.0	0.0	0.00
	04/03/90	EMS	A204067	0.0	-250.0	-250.0	6100.00	-250.0	2900.00	6200.0	-250.0	0.0	0.00
	07/20/90	EMS	A210736	0.0	-5.0	-5.0	3800.00	-5.0	120.00	84.0	-5.0	0.0	0.00
	10/15/90	EMS	A216232	0.0	-5.0	7.0	4900.00	-5.0	800.00	140.0	-5.0	0.0	0.00
RW-4	01/31/90	EMS	A200238	0.0	-5.0	-5.0	1800.00	-5.0	390.00	14.0	-5.0	0.0	0.00
	04/03/90	EMS	A204065	0.0	-5.0	-5.0	2700.00	-5.0	900.00	44.0	-5.0	0.0	0.00
	07/20/90	EMS	A210737	0.0	-5.0	-5.0	2000.00	-5.0	650.00	22.0	-5.0	0.0	0.00
	10/15/90	EMS	A216234	0.0	-5.0	8.0	9500.00	-5.0	800.00	900.0	-5.0	0.0	0.00
RW-5	01/31/90	EMS	A200239	0.0	6.0	-5.0	-5.00	-5.0	-5.00	-5.0	-5.0	0.0	0.00
	04/12/90	EMS	A204064	0.0	5.0	-5.0	-5.00	-5.0	-5.00	-5.0	-5.0	0.0	0.00
	07/20/90	EMS	A210738	0.0	-5.0	-5.0	12.00	-5.0	6.00	-10.0	-5.0	0.0	0.00
	10/15/90	EMS	A216235	0.0	-5.0	-5.0	2000.00	-5.0	500.00	27.0	-5.0	0.0	0.00
	02/06/91*	EMS	A222385	0.0	-5.0	-5.0	210.00	-5.0	8.00	130.0	-5.0	0.0	0.00

Well	Sample Collection Date	Laboratory	Laboratory Report Number	TOC (µg/L)	Toluene (µg/L)	1,1-DCE (μg/L)	t-1,2- DCE (μg/L)	1,1,1- TCA (µg/L)	TCE (µg/L)	Vinyl Chloride (µg/L)	1,2-DCA (µg/L)	Silver (µg/L)	pН
MS-1	09/01/88	metaTRACE	AA17388	0.0	-5.0	-5.0	25.00	-5.0	15.00	-10.0	50	The state of the s	
	10/12/88	metaTRACE	AA20406	0.0	-5.0	0.0	9.40	-5.0	160.00	-10.0	-5.0 -2500.0	0.0	0.00
	02/09/90	EMS	A200912	0.0	-5.0	-5.0	840.00	-5.0	35.00	-10.0	-2500.0 29.0	0.0	0.00
	04/04/90	EMS	A204073	0.0	5.0	-5.0	2800.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	07/19/90	EMS	A210627	0.0	-5.0	6.0	5800.00	-5.0	1900.00	18.0	-5.0	0.0	0.00
	10/11/90	EMS	A216154	0.0	-5.0	-5.0	5600.00	-5.0	8000.00	-10.0	-5.0	0.0	0.00
MS-2	09/01/88	metaTRACE	AA17389	0.0	7.0	29.0	15000.00	-5.0	98000.00	-10.0	-5.0	0.0	0.00
	10/12/88	Wilson	88110211	0.0	-2500.0	-2500.0	13000.00	-2500.0	44000.00	-5000.0	-5.0	0.0	0.00
	10/12/88	metaTRACE	AA20407	0.0	6.2	8.0	7800.00	-5.0	30000.00	72.0	-5.0	0.0	0.00
	02/09/90	EMS	A200914	0.0	-5.0	-5.0	14000.00	-5.0	42000.00	-10.0	-5.0	0.0	0.00
	04/03/90	EMS	A204073	0.0	-2500.0	-2500.0	6300.00	-2500.0	9300.00	-5000.0	-2500.0	0.0	0.00
	07/19/90	EMS	A210617	0.0	-5.0	6.0	9800.00	-5.0	17000.00	35.0	-5.0	0.0	0.00
	10/11/90	EMS	A216152	0.0	-5.0	16.0	8400.00	-5.0	19000.00	35.0	-5.0	0.0	0.00
MS-3	09/02/88	metaTRACE	AA17391	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/12/88	metaTRACE	AA20408	0.0	-5.0	-5.0	110.00	-5.0	230.00	-10.0	-5.0	0.0	0.00
	02/09/90	EMS	A200910	0.0	-5.0	-5.0	39.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	04/04/90	EMS	A204071	0.0	-5.0	-5.0	30.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	07/19/90	EMS	A210623	0.0	-5.0	-5.0	50.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/15/90	EMS	A216228	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	34.0	0.0	0.00
MS-4	09/01/88	metaTRACE	AA17390	0.0	-5.0	-5.0	100.00	-5.0	210.00	-10.0	-5.0	0.0	0.00
	10/12/88	metaTRACE	AA20409	0.0	-5.0	-5.0	-5.00	-5.0	56.00	-10.0	-5.0	0.0	0.00
	10/27/88	metaTRACE	AA21035	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/27/88	metaTRACE	AA21036	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00

Well	Sample Collection Date	Laboratory	Laboratory Report Number	TOC (μg/L)	Toluene (µg/L)	1,1-DCE (µg/L)	t-1,2- DCE (μg/L)	1,1,1- ΤCA (μg/L)	TCE (µg/L)	Vinyl Chloride (µg/L)	1,2-DCA (μg/L)	Silver (µg/L)	рН
MS-5	01/18/89	NET	39507	0.0	-1.0	-1.0	-1.00	-1.0	74.40	20.0	4.0		
	06/07/89	NET	42192	0.0	-1.0	-1.0	-1.00	-1.0	74.40	-20.0	-1.0	0.0	0.00
	02/09/90	EMS	A200915	0.0	-5.0	-5.0	21.00	-5.0	27.50	-20.0	-1.0	0.0	0.00
	04/04/90	EMS	A204074	0.0	-5.0	-5.0	24.00	-5.0	35.00 19.00	-10.0	-5.0	0.0	0.00
	07/19/90	EMS	A210624	0.0	-5.0	-5.0	14.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/11/90	EMS	A216157	0.0	-5.0	-5.0	30.00	-5.0	20.00	-10.0 -10.0	-5.0 -5.0	0.0 0.0	0.00
MS-6	12/05/88	NET	38639	0.0	-1.0	-1.0	-1.0	-1.0	-1.00	-20.0	-1.0	0.0	0.00
	06/07/89	NET	42193	0.0	-1.0	-1.0	-1.00	-1.0	-1.00	-20.0	-1.0	0.0	0.00
	02/09/90	EMS	A200911	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	04/04/90	EMS	A204072	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	07/19/90	EMS	A210743	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/11/90	EMS	A216153	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
MD-1	08/26/88	metaTRACE	AA16900	0.0	0.0	0.0	0.16	0.0	0.61	0.0	0.0	0.0	0.00
	09/01/88	metaTRACE	AA17382	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/12/88	Wilson	88110208	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/12/88	metaTRACE	AA20403	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	03/13/90	EMS	A202547	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	04/03/90	EMS	A204069	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-5.0	-5.0	0.0	0.00
	07/20/90	EMS	A210740	0.0	-5.0	-5.0	-5.00	-5.0	8.00	-10.0	-5.0	0.0	0.00
	08/21/90*	EMS	A210429	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/15/90	EMS	A216230	0.0	-5.0	-5.0	9.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	01/24/91*	EMS	A222562	0.0	-5.0	-5.0	8.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00

Well	Sample Collection Date	Laboratory	Laboratory Report Number	TOC (µg/L)	Toluene (µg/L)	1,1-DCE (μg/L)	t-1,2- DCE (µg/L)	1,1,1- TCA (µg/L)	TCE (µg/L)	Vinyl Chloride (µg/L)	1,2-DCA (μg/L)	Silver (µg/L)	pН
MD-2	08/26/88	metaTRACE	AA16901	0.0	0.0	0.0	2.72	0.0	1.06	0.0		*************	
	09/01/88	metaTRACE	AA17383	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	0.0	0.0	0.0	0.00
	10/12/88	metaTRACE	AA20404	0.0	-5.0	-5.0	-5.00	-5.0 -5.0	-5.00 -5.00	-10.0 -10.0	-5.0	0.0	0.00
	10/12/88	Wilson	88110209	0.0	-5.0	-5.0	-5.00	-5.0	-5.00		-5.0	0.0	0.00
	03/13/90	EMS	A202548	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0 -10.0	-5.0	0.0	0.00
	04/03/90	EMS	A204068	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	07/20/90	EMS	A210741	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/11/90	EMS	A216156	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0 -5.0	0.0	0.00
MD-3	08/26/88	metaTRACE	AA16901	0.0	0.0	0.0	0.65	0.0	0.05	0.0	0.0	0.0	0.00
	09/01/88	metaTRACE	AA17384	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/12/88	Wilson	88110210	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/12/88	metaTRACE	AA20405	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/27/88	metaTRACE	AA21039	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/27/88	metaTRACE	AA21038	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
SS-2	04/12/90	EMS	A204648	0.0	-5.0	-5.0	260.00	-5.0	76.00	-10.0	-5.0	0.0	0.00
	07/19/90	EMS	A210626	0.0	-5.0	-5.0	38.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/11/90	EMS	A216155	0.0	-5.0	-5.0	2300.00	-5.0	230.00	-10.0	-5.0	0.0	0.00
SS-3	07/19/90	EMS	A210625	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/15/90	EMS	A216229	0.0	-5.0	-5.0	-5.00	-5.0	19.00	-10.0	-5.0	0.0	0.00
MW-1	12/05/88	NET	38583	0.0	0.0	0.0	0.00	0.0	4.60	0.0	-5.0	0.0	0.00
	01/18/89	NET	39501	6000	-1.0	-1.0	-1.00	-1.0	64.10	-20.0	-1.0	0.0	6.24
	06/06/89	NET	42156	14000	-1.0	-1.0	-1.00	-1.0	84.00	-20.0	-1.0	0.0	0.00
	09/28/89	NET	44980	8000	-1.0	-1.0	-1.00	-1.0	39.40	-20.0	-1.0	0.0	0.00

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MW-1 (cont.)	12/20/89	Well dry		0.0	0.0	0.0	0.00	0.0	0.00	0.0	0.0	0.0	0.00
,	02/02/90	EMS	A201954	26000	-5.0	-5.0	-5.00	-5.0	64.00	-5.0	-5.0	0.0	0.00
	04/13/90	EMS	A204636	11000	-5.0	-5.0	-5.00	-5.0	23.00	-10.0	-5.0 -5.0	0.0	0.00
	07/19/90	EMS	A210618	5000	-5.0	-5.0	-5.00	-5.0	39.00	-10.0	-5.0	0.0	0.00
	10/11/90	EMS	A216148	4000	-5.0	-5.0	-5.00	11.0	24.00	-5.0	-5.0 -5.0	0.0	0.00
MW-2	12/05/88	NET	38584	0.0	0.0	0.0	0.00	0.0	353.00	0.0	0.0	0.0	0.00
	01/18/89	Continental	89010514	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	5.0	-5.0	0.0	0.00
	01/18/89	NET	39502	4000	-1.0	-1.0	-1.00	-1.0	-1.00	-20.0	-1.0	0.0	
	06/06/89	NET	42157	9000	-1.0	-1.0	-1.00	-1.0	-1.00	-20.0	-1.0	0.0	6.28
	09/28/89	NET	44891	6000	-1.0	-1.0	-1.00	-1.0	-1.00	-20.0	-1.0		0.00
	12/20/89	EMS	137000	-3000	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	03/02/90	EMS	A201955	-3000	-5.0	-5.0	-5.00	-5.0	-5.00	-5.0	-5.0	0.0	0.00
	04/12/90	EMS	A204642	-3000	-5.0	-5.0	8.00	-5.0	23.00	-10.0	-5.0	0.0 0.0	0.00
	06/08/90	EMS	A208451	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	07/18/90	EMS	A210614	-3000	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/11/90	EMS	A216145	-3000	-5.0	-5.0	-5.00	11.0	24.00	-10.0	-5.0	0.0	0.00
MW-3	12/05/88	NET	38585	0.0	0.0	0.0	0.00	0.0	97.70	0.0	0.0	0.0	0.00
	01/18/89	NET	39503	-1000	-10.0	-10.0	-10.00	-10.0	1280.00	-200.0	-10.0	0.0	6.76
	06/06/89	NET	42158	278000	-1.0	-1.0	-1.00	2.4	531.00	-20.0	-10.0	0.0	0.00
	09/28/89	NET	44892	6000	-1.0	-1.0	-1.00	1.2	158.00	20.0	-1.0	0.0	0.00
	12/20/89	Well dry		0.0	0.0	0.0	0.00	0.0	0.00	0.0	0.0	0.0	0.00
	03/02/90	EMS	A201956	-3000	-5.0	-5.0	16.00	-5.0	380.00	-5.0	-5.0	0.0	0.00
	04/12/90	EMS	A204637	4000	-5.0	-5.0	5.00	-5.0	150.00	-10.0	-5.0	0.0	0.00
	07/18/90	EMS	A210615	5000	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/11/90	EMS	A216146	5000	-5.0	-5.0	6.50	-5.0	69.00	-10.0	-5.0	0.0	0.00

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MW-4	12/05/88	NET	38586	0.0	0.0	0.0	0.00	0.0	638.00	0.0	0.0		
	01/18/89	NET	39504	-1000	-1.0	-1.0	-1.00	1.3	167.00	0.0	0.0	0.0	0.00
	01/18/89	Continental	89010515	0.0	-5.0	-5.0	-5.00	-5.0	91.00	-20.0 -5.0	-1.0	0.0	6.50
	06/06/89	NET	42159	161000	-1.0	-1.0	2.50	2.7	438.00	-3.0	-5.0	0.0	0.00
	09/28/89	NET	44983	6000	-1.0	-1.0	-1.00	1.6	194.00	-20.0	-1.0	0.0	0.00
	12/20/89	EMS	137001	32000	-5.0	-5.0	54.00	-5.0	210.00	-20.0	-1.0 -5.0	0.0	0.00
	03/02/90	EMS	A201957	-3000	-5.0	-5.0	-5.00	-5.0	560.00	-5.0	-5.0	0.0	0.00
	04/13/90	EMS	A204638	4000	-5.0	-5.0	-5.00	-5.0	330.00	-10.0	-5.0 -5.0	0.0	0.00
	07/18/90	EMS	A210616	5000	-5.0	-5.0	-5.00	-5.0	220.00	-10.0	-5.0	0.0	0.00
	10/11/90	EMS	A216147	6000	-5.0	-5.0	-5.00	-5.0	310.00	-10.0	-5.0	0.0	0.00
1W-5	12/05/88	NET	38587	0.0	0.0	0.0	0.00	0.0	272.00	0.0	-5.0	0.0	0.00
	01/18/89	NET	39505	-1000	-100.0	-100.0	-100.00	-100.0	12200.00	-2000.0	-100.0	0.0	0.00
	06/06/89	NET	42160	288000	-1.0	-1.0	896.00	-1.0	319.00	-2000.0		0.0	6.62
	09/28/89	NET	44489	30000	-1.0	31.4	131.00	-1.0	713.00	-20.0	-1.0	0.0	0.00
	12/20/89	EMS	137003	43000	-5.0	12.0	6000.00	-5.0	150.00		-1.0	0.0	0.00
	03/02/90	EMS	A201958	9000	-5.0	12.0	11000.00	-5.0	11.00	38.0	-5.0	0.0	0.00
	04/12/90	EMS	A204643	-3000	-5.0	-5.0	1100.00	-5.0		4500.0	-5.0	0.0	0.00
	07/18/90	EMS	A210619	-3000	-5.0	-5.0	410.00	-5.0	140.00	10.0	-5.0	0.0	0.00
	10/11/90	EMS	A216151	4000	-5.0	-5.0	520.00		130.00	-10.0	-5.0	0.0	0.00
	10/11/20	Ling	71210131	400	-5.0	-3.0	320.00	-5.0	62.00	14.0	-5.0	0.0	0.00
1W-6	12/05/88	NET	38588	0.0	-5.0	0.0	0.00	0.0	2.60	0.0	0.0	0.0	0.00
	01/18/89	Continental	89010516	0.0	-5.0	-5.0	-5.00	-5.0	1600.00	-5.0	-5.0	0.0	0.00
	01/18/89	NET	39506	-1000	-100.0	-100.0	-100.00	-100.0	4600.00	-2000.0	-100.0	0.0	6.71
	06/06/89	NET	42161	61000	-1.0	-1.0	1030.00	3.7	2590.00	-20.0	-1.0	0.0	0.00
	09/28/89	NET	44489	19000	-1.0	4.5	13.50	2.0	760.00	-20.0	-1.0	0.0	0.00
	12/20/89	EMS	137002	52000	-5.0	-5.0	680.00	-5.0	3100.00	-10.0	-5.0	0.0	0.00
	03/02/90	EMS	A201959	-3000	-5.0	-5.0	1000.00	-5.0	4900.00	-5.0	6.0	0.0	0.00

Well	Sample Collection Date	Laboratory	Laboratory Report Number	TOC (µg/L)	Toluene (µg/L)	1,1-DCE (μg/L)	t-1,2- DCE (μg/L)	1,1,1- TCA (µg/L)	TCE (µg/L)	Vinyl Chloride (µg/L)	1,2-DCA (µg/L)	Silver (µg/L)	рН
MW-6 (cont.)	04/13/90	EMS	A204639	6000	6.0	5.0	1000.00	-5.0	3300.00	10.0	82.0	0.0	0.00
,	07/18/90	EMS	A210620	4000	-5.0	9.0	3300.00	-5.0	6800.00	-10.0	-5.0	0.0	0.00
	10/11/90	EMS	A216149	6000	-5.0	8.3	2700.00	11.0	7400.00	-10.0	8.3	0.0	0.00
Stripper													
Effluent	01/31/90	EMS	A200241	9000	-5.0	-5.0	66.00	-5.0	-5.00	-10.0	-5.0	-10	7.50
	03/02/90	EMS	A200962	4000	-5.0	-5.0	49.00	-5.0	-5.00	-10.0	-5.0	13	0.00
	04/04/90	EMS	A204078	-3000	-5.0	-5.0	36.00	-5.0	-5.00	-10.0	-5.0	-10	6.50
	06/08/90	EMS	A208452	23000	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	-10	0.00
	07/20/90	EMS	A210745	4000	-5.0	-5.0	27.00	-5.0	52.00	-10.0	-5.0	-10	8.00
	09/26/90	EMS	A214777	4000	5.0	-5.0	59.00	-5.0	-5.00	-5.0	-5.0	-10	8.0
	10/12/90	EMS	A216160	4000	-5.0	-5.0	67.00	-5.0	-5.00	-10.0	-5.0	-10	8.1
	11/30/90	EMS	A219266	10000	5.0	-5.0	8.00	-5.0	-5.00	-5.0	-5.0	-10	8.00
	12/28/90	EMS	A222141	-3000	5.0	-5.0	180.00	-5.0	-5.00	70.0	-5.0	-10	8.30
Stripper													
Influent	01/31/90	EMS	A200240	0.0	-5.0	14.0	7900.00	-5.0	170.00	170.0	-5.0	0.0	0.00
Field Blank	09/01/88	metaTRACE	AA17387	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	09/01/88	metaTRACE	AA17386	0.0	-5.0	-5.00	-5.0	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/12/88	metaTRACE	C299	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/12/88	metaTRACE	AA20410	0.0	-5.0	-5.0	-5.00	-5.0	21.00	-10.0	-5.0	0.0	0.00
	10/12/88	Wilson	88110212	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.0
	10/27/88	metaTRACE	AA21037	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.0
	12/05/88	NET	38590	0.0	-1.0	-1.0	-1.00	-1.0	-1.00	-20.0	-1.0	0.0	0.0
	01/18/89	NET	39509	0.0	-1.0	-1.0	-1.00	-1.0	10.30	-20.0	-1.0	0.0	0.0
	06/06/89	NET	42162	0.0	1.3	-1.0	-1.00	-1.0	11.70	-20.0	-1.0	0.0	0.00

Well	Sample Collection Date	Laboratory	Laboratory Report Number	TOC (µg/L)	Toluene (µg/L)	1,1-DCE (µg/L)	t-1,2- DCE (µg/L)	1,1,1- ΤCA (μg/L)	TCE (µg/L)	Vinyl Chloride (µg/L)	1,2-DCA (µg/L)	Silver (µg/L)	рН
Field Blank	06/06/89	NET	42163	0.0	1.4	-1.0	-1.00	-1.0	2.90	-20.0	-1.0	0.0	0.00
(cont.)	09/28/89	NET	44979	0.0	-1.0	-1.0	-1.00	-1.0	-1.00	-20.0	-1.0	0.0	0.00
	12/20/89	EMS	8946084	-3,000	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	02/09/90	EMS	A200916	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	03/02/90	EMS	A201961	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-5.0	-5.0	0.0	0.00
	03/13/90	EMS	A202549	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	04/04/90	EMS	A204076	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	04/13/90	EMS	A204641	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-5.0	-5.0	0.0	0.00
	07/20/90	EMS	A210746	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00
	10/11/90	EMS	A216159	0.0	-5.0	-5.0	-5.00	-5.0	-5.00	-10.0	-5.0	0.0	0.00

Resampled

μg/L Micrograms per liter

TOC Total organic carbons TCE Trichloroethylene

1,1-DCE 1,1-Dichloroethylene

1,2-DCA 1,2-Dichloroethane

1,1,1-TCA 1,1,1-Trichloroethane

t-1,2-DCE trans-1,2-Dichloroethylene

Chemical Analyses for Hussmann-SECO, Washington, Missouri.

Negative values indicate the measured constituent was below the detection limit. Zero indicates the constituent was not included in the analysis.

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
RW-1	12/06/88	482.93	13.29	469.64		
	01/17/89	482.93	22.63	460.30		
	06/07/89	482.93	20.72	462.21		
	09/13/89	482.93	14.33	468.60		
	09/28/89	482.93	19.62	463.31		
	11/10/89	482.93	19.07	463.86		
	01/29/90	479.82	21.76	458.06		
	01/30/90	479.82	28.49	451.33	7.0	6,710
	01/31/90	479.82	30.14	449.68	7.0	16,235
	02/01/90	479.82	30.91	448.91	7.0	26,970
	02/02/90	479.82	30.60	449.22	7.0	
	02/22/90	479.82	24.20	455.62	7.0	
	03/01/90	479.82	20.71	459.11	7.5	163,623
	03/02/90	479.82	24.24	455.58	8.0	
	03/13/90	479.82	28.26	451.56		197,200
	04/03/90	479.82	12.42	467.40		197,201
	04/12/90	479.82	12.39	467.43		197,201
	07/18/90	479.82	22.70	457.12		200,722
	08/06/90	479.82	22.40	457.42		222,589
	10/15/90	479.82	26.37	453.45		222,589

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
RW-2	√11/10/89	479.14	18.79	460.35		
	01/29/90	479.14	21.31	457.83		
	01/30/90	479.14	23.52	455.62	11.5	12,855
	01/31/90	479.14	21.98	457.16	10.0	21,063
	02/01/90	479.14	25.07	454.07	19.5	48,450
	02/02/90	479.14	25.21	453.93	20.0	
	02/09/90	479.14	27.00	452.14	20.8	252,572
	02/22/90	479.14	24.50	454.64	18.0	
	03/01/90	479.14	22.29	456.85	20.0	895,778
	03/02/90	479.14	22.29	456.85	22.0	
	03/13/90	479.14	22.50	456.64	20.5	1,246,240
	04/03/90	479.14	17.81	461.33	19.4	1,872,040
	04/12/90	479.14	18.25	460.89		2,101,050
	07/18/90	479.14	17.39	461.75		-,
	08/06/90	479.14	17.40	461.74	23.0	
	10/15/90	479.14	23.64	455.50	26.5	
RW-3	√11/10/89	478.91	16.00	462.91		
	01/29/90	478.91	16.82	462.09		
	01/30/90	478.91	41.68	437.23	8.0	8,830
	01/31/90	478.91	37.11	441.80	8.8	19,010
	02/01/90	478.91	40.64	438.27	9.5	33,060
	02/02/90	478.91	42.91	436.00	10.0	

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
RW-3 (cont.)	02/09/90	478.91	42.90	436.01	10.6	135,607
,	02/22/90	478.91	42.20	436.71	10.0	133,007
	03/01/90	478.91	34.83	444.08	11.0	452,495
	03/02/90	478.91	42.44	436.47	12.0	132,173
	03/13/90	478.91	42.92	435.99	11.6	652,460
	04/03/90	478.91	36.58	442.33	13.5	1,004,800
	04/12/90	478.91	37.46	441.45	11.5	1,153,410
	07/18/90	478.91	24.00	454.91		2,110,473
	08/06/90	478.91	26.20	452.71	5.5	2,250,210
	10/15/90	478.91	35.80	442.11	6.1	2,515,462
RW-4	√11/10/89	483.84	21.82	462.02		
	01/29/90	483.84	24.08	459.76		
	01/30/90	483.84	31.62	452.22	1.8	1,420
	01/31/90	493.84	25.03	458.81	0.8	1,714
	02/01/90	483.84	32.71	451.13	1.5	3,324
	02/02/90	483.84	32.65	451.19	1.3	
	02/22/90	483.84	25.00	458.84		
	03/01/90	483.84	32.29	451.55	0.8	24,900
	03/02/90	483.84	32.71	446.63	1.5	
	03/13/90	483.84	35.00	448.84	2.0	56,730
	04/03/90	483.84	25.85	457.99	0.8	83,780

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
RW-4 (cont.)	04/12/90	483.84	23.54	460.30	0.7	103,310
(07/18/90	483.84	34.84	449.00	3.0	238,214
	08/06/90	483.84	30.82	453.02	2.5	300,091
	10/15/90	493.84	34.78	449.06	2.1	394,170
RW-5	11/10/89	486.84	21.68	465.16		
	01/29/90	486.84	22.37	464.47		15,863
	01/30/90	486.84	34.34	452.50		15,892
	01/31/90	486.84	35.72	451.12		15,900
	02/01/90	486.84	33.84	453.00		15,901
	02/02/90	486.84	32.29	454.55		
	02/22/90	486.84	31.70	455.14		
	03/01/90	486.84	33.21	453.63		16,200
	03/02/90	486.84	35.62	451.22		
	03/13/90	486.84	35.81	451.03		16,315
	04/03/90	486.84	35.83	451.01		16,520
	04/12/90	486.84	35.71	451.13		
	07/18/90	486.84	34.25	452.59		24,414
	08/06/90	486.84	18.97	467.87		24,503
	10/15/90	486.87	20.42	466.42		24,503

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
MS-1	10/12/88	482.32	20.69	461.63		
	10/26/88	482.32	21.01	461.31		
	11/30/88	482.32	20.27	462.05		
	12/06/88	482.32	20.34	461.98		
	01/17/89	482.32	20.90	461.42		
	06/07/89	482.32	19.10	463.22		
	09/13/89	482.32	14.63	467.69		
	09/28/89	482.32	18.14	464.18		
	√11/10/89	482.32	20.57	461.75		
	01/29/90	482.32	22.82	459.50		
	01/30/90	482.32	24.35	457.97		
	01/31/90	482.32	24.95	457.37		
	02/01/90	482.32	24.86	457.46		
	02/02/90	482.32	25.01	457.31		
	02/09/90	482.32	24.50	457.82		
	02/22/90	482.32	23.50	458.82		
	03/01/90	482.32	23.04	459.28		
	03/13/90	482.32	23.90	458.42		
	04/03/90	482.32	18.40	463.92		
	04/12/90	482.32	18.65	463.67		
	07/18/90	482.32	18.23	464.09		
	✓ 10/12/90	482.32	22.28	460.04		

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
MS-2	10/12/88	482.75	22.45	460.30		
	10/26/88	482.75	22.76	459.99		
	11/30/88	482.75	21.91	460.84		
	12/06/88	482.75	22.17	460.58		
	01/17/89	482.75	22.96	459.79		
	06/07/89	482.75	20.82	461.93		
	09/13/89	482.75	13.77	468.98		
	09/28/89	482.75	19.72	463.03		
	√ 11/10/89	482.75	22.27	460.48		
	01/29/90	482.75	24.80	457.95		
	01/30/90	482.75	25.66	457.09		
	01/31/90	482.75	25.50	457.25		
	02/01/90	482.75	26.25	456.50		
	02/02/90	482.75	26.37	456.38		
	02/09/90	482.75	26.30	456.45		
	02/22/90	482.75	25.20	457.55		
	03/01/90	482.75	23.35	459.40		
	03/13/90	482.75	23.54	459.21		
	04/03/90	482.75	18.77	463.98		
	04/12/90	482.75	19.23	463.52		
	07/18/90	482.75	18.54	464.21		
	10/12/90	482.75	23.88	458.87		

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
MS-3	10/12/88	491.77	26.66	465.11		
	10/26/88	491.77	26.72	465.05		
	06/07/89	491.77	29.56	462.21		
	09/13/89	491.77	24.67	467.10		
	09/28/89	491.77	27.28	464.49		
	11/10/89	491.77	28.18	463.59		
	01/29/90	492.75	28.55	464.20		
	01/30/90	492.75	28.50	464.25		
	01/31/90	492.75	28.55	464.20		
	02/01/90	492.75	28.38	464.37		
	02/02/90	492.75	28.60	464.15		
	02/09/90	492.75	30.10	462.65		
	02/22/90	492.75	28.20	464.55		
	03/01/90	492.75	27.75	465.00		φ.
	03/13/90	492.75	28.17	464.58		
	04/03/90	492.75	25.88	466.87		
	04/12/90	492.75	25.83	466.92		
	07/18/90	492.75	24.11	468.64		
	10/12/90	492.75	27.00	465.75		
MS-4	10/12/88	493.17	27.58	465.59		
	10/26/88	493.17	27.66	465.51		

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
MS-5	12/06/88	491.95	29.29	462.66		
	01/17/89	491.95	29.63	462.32		
	06/07/89	491.95	28.14	463.81		
	09/13/89	491.95	25.03	466.92		
	09/28/89	491.95	27.29	464.66		
	11/10/89	491.95	29.57	462.38		
	01/29/90	491.95	31.66	460.29		
	01/30/90	491.95	32.83	459.12		
	01/31/90	491.95	32.48	459.47		
	02/01/90	491.95	33.33	458.62		
	02/02/90	491.95	33.61	458.34		
	02/09/90	491.95	32.90	459.05		
	02/22/90	491.95	32.50	459.45		
	03/01/90	491.95	32.85	459.10		
	03/13/90	491.95	33.35	458.60		
	04/03/90	491.95	23.29	468.66		
	04/12/90	491.95	28.29	462.66		
	07/18/90	491.95	27.68	464.27		
	10/12/90	491.95	31.39	460.56		
MS-6	12/06/88	492.15	26.45	465.70		
	01/17/89	492.15	23.64	468.51		
	06/07/89	492.15	23.66	468.49		
	09/13/89	492.15	24.83	467.32		

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
MS-6 (cont.)	09/28/89	492.15	24.71	467.44		
, ,	√ 11/10/89	492.15	25.26	466.89		
	01/29/90	492.15	25.84	466.31		
	01/30/90	492.15	25.72	466.43		
	01/31/90	492.15	25.85	466.30		
	02/01/90	492.15	25.79	466.36		
	02/02/90	492.15	25.78	466.37		
	02/09/90	492.15	25.50	466.65		
	02/22/90	492.15	26.10	466.05		
	03/01/90	492.15	25.42	466.73		
	03/13/90	492.15	24.98	467.17		
	04/03/90	492.15	23.94	468.21		
	04/12/90	492.15	23.79	468.36		
	07/18/90	492.15	20.65	471.50		
	10/11/90	492.1	23.19	468.96		
MD-1	10/12/88	482.62	21.02	461.60		
	10/26/88	482.62	21.29	461.33		
	11/30/88	482.62	21.22	461.40		
	12/06/88	482.62	20.93	461.69		
	01/17/89	482.62	21.54	461.08		
	06/07/89	482.62	20.10	462.52		
	09/13/89	482.62	17.49	465.13		

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
MD-1 (cont.)	09/28/89	482.62	18.99	463.63		
(/	11/10/89	482.62	21.19	461.43		
	01/29/90	482.62	23.20	459.42		
	01/30/90	482.62	23.08	459.54		
	01/31/90	482.62	23.36	459.26		
	02/01/90	482.62	23.18	459.44		
	02/02/90	482.62	23.25	459.37		
	02/09/90	482.62	19.20	463.42		
	02/22/90	482.62	23.10	459.52		
	03/01/90	482.62	22.00	460.62		
	03/13/90	482.62	21.46	461.16		
	04/03/90	482.62	18.60	464.02		
	04/12/90	482.62	18.77	463.85		
	07/18/90	482.62	15.19	467.43		
	10/15/90	482.62	20.03	462.59		
MD-2	10/12/88	482.58	19.89	462.69		
	10/26/88	482.58	19.99	462.59		
	11/30/88	482.58	20.02	462.56		
	12/06/88	482.58	29.83	452.75		
	01/17/89	482.58	20.24	462.34		
	06/07/89	482.58	19.34	463.24		
	09/13/89	482.58	19.02	463.56		

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
MD-2 (cont.)	09/28/89	482.58	18.31	464.27		Bottom of Wall
()	11/10/89	482.58	20.15	462.43		
	01/29/90	482.58	21.98	460.60		
	01/30/90	482.58	21.85	460.73		
	01/31/90	482.58	22.15	460.43		
	02/01/90	482.58	21.92	460.66		
	02/02/90	482.58	22.00	460.58		
	02/09/90	482.58	22.10	460.48		
	02/22/90	482.58	22.30	460.28		
	03/01/90	482.58	21.75	460.83		
	03/13/90	482.58	21.06	461.52		
	04/03/90	482.58	18.75	463.83		
	04/12/90	482.58	18.83	463.75		
	07/18/90	482.58	13.93	468.65		
	10/12/90	482.58	18.15	464.43		
MD-3	10/12/88	493.43	30.12	463.31		
	10/26/88	493.43	30.21	463.22		
SS-1	12/06/88	483.22	17.51	465.71 ⁰	RY?	
	07/18/90	483.22	16.37	466.85	crasne 462	465 ±

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
SS-2	12/06/88	483.88	21.56	462.32		Butters of well
	01/17/89	483.88	21.96	461.92 Ory	>	
	06/07/89	483.88	20.35	463.53	•	
	09/13/89	483.88	17.23		sh 10 474	
	09/28/89	483.88	19.30	464.58	445	
	07/18/90	483.88	17.48	466.40		
	10/12/90	483.88	21.12	462.76		
SS-3	12/06/88	492.14	22.33	469.81		47132
	07/18/90	492.14	20.31	10	159	
	10/12/90	492.14	22.12		162	
MW-1	10/12/88	482.02	21.30	460.72		
	10/26/88	482.02	21.56	460.46		
	11/30/88	482.02	18.24	463.78		
	12/06/88	482.02	20.23	461.79		
	01/17/89	482.02	20.16	461.86		
	06/06/89	482.02	16.92	465.10		
	06/07/89	482.02	17.08	464.94		
	09/13/89	482.02	15.02	467.00		
	09/28/89	482.02	17.44	464.58		
	√11/10/89	482.02	21.27	460.75		
	03/01/90	482.02	22.58	459.44		

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
MW-1 (cont.)	03/13/90	482.02	22.64	459.38		
(04/03/90	482.02	15.62	466.40		
	04/12/90	482.02	15.75	466.27		
	07/18/90	482.02	13.26	468.76		
	10/11/90	482.02	11.82	470.20		
MW-2	10/12/88	494.94	25.64	469.30		
	10/26/88	494.94	25.83	469.11		
	11/30/88	494.94	25.62	469.32		
	12/06/88	492.43	22.41	470.02		
	01/17/89	492.43	22.41	470.02		
	06/06/89	492.43	21.93	470.50		
	06/07/89	492.43	21.78	470.65		
	09/13/89	492.43	22.45	469.98		
	09/28/89	492.43	22.64	469.79		
	11/10/89	492.43	23.42	469.01		
	01/29/90	492.43	24.26	468.17		
	01/30/90	492.43	24.29	468.14		
	01/31/90	492.43	24.29	468.14		
	02/01/90	492.43	24.29	468.14		
	03/01/90	492.43	18.90	473.53		
	03/13/90	492.43	23.75	468.68		

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
MW-2 (cont.)	04/03/90	492.43	22.52	469.91		
(04/12/90	492.43	22.51	469.92		
	07/18/90	492.43	18.28	474.15		
	10/11/90	492.43	21.85	470.58		
MW-3	10/12/88	482.81	21.49	461.32		
	10/26/88	482.81	21.63	461.18		
	11/30/88	482.81	18.41	464.40		
	12/06/88	482.81	19.71	463.10		
	01/17/89	482.81	19.26	463.55		
	06/06/89	482.81	17.49	465.32		
	06/07/89	482.81	18.05	464.76		
	09/13/89	482.81	16.32	466.49		
	09/28/89	482.81	17.15	465.66		
	11/10/89	482.81	21.12	461.69		
	03/01/90	482.81	22.08	460.73		
	03/13/90	482.81	22.06	460.75		
	04/03/90	482.81	16.29	466.52		
	04/12/90	482.81	16.40	466.41		
	07/18/90	482.81	12.96	469.85		
	10/11/90	482.81	18.21	464.60		

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
MW-4	10/12/88	481.83	17.90	463.93		
	10/26/88	481.83	17.74	464.09		
	11/30/88	481.83	14.31	467.52		
	12/06/88	481.83	16.11	465.72		
	01/17/89	481.83	13.62	468.21		
	06/06/89	481.83	13.71	468.12		
	06/07/89	481.83	14.05	467.78		
	09/13/89	481.83	14.82	467.01		
	09/28/89	481.83	15.34	466.49		
	11/10/89	481.83	18.25	463.58		
	01/29/90	481.83	22.03	459.80		
	01/30/90	481.83	23.02	458.81		
	01/31/90	481.83	23.15	458.68		
	02/09/90	481.83	22.70	459.13		
	02/22/90	481.83	20.80	461.03		
	03/01/90	481.83	17.29	464.54		
	03/13/90	481.83	17.79	464.04		
	04/03/90	481.83	13.77	468.06		
	04/12/90	481.83	13.67	468.16		
	07/18/90	481.83	11.28	470.55		
	10/11/90	481.83	14.18	467.65		

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
MW-5	10/12/88	484.24	24.07	460.17		
	10/26/88	484.24	24.35	459.89		
	11/30/88	484.24	23.56	460.68		
	12/06/88	484.24	23.86	460.38		
	01/17/89	484.24	24.64	459.60		
	06/06/89	484.24	22.25	461.99		
	06/07/89	484.24	22.37	461.87		
	09/13/89	484.24	15.72	468.52		
	09/28/89	484.24	20.94	463.30		
	V11/10/89	484.24	23.82	460.42		
	01/29/90	484.24	26.37	457.87		
	01/30/90	484.24	27.20	457.04		
	01/31/90	484.24	27.04	457.20		
	02/01/90	484.24	27.80	456.44		
	02/02/90	484.24	27.91	456.33		
	02/22/90	484.24	27.00	457.24		
	03/01/90	484.24	24.95	459.29		
	03/13/90	484.24	25.14	459.10		
	04/03/90	484.24	20.04	464.20		
	04/12/90	484.24	20.59	463.65		
	07/18/90	484.24	19.85	464.39		
	10/11/90	484.24	25.38	458.86		

Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
MW-6	10/12/88	493.37	26.86	466.51		
	10/26/88	493.37	26.69	466.68		
	11/30/88	493.37	25.40	467.97		
	12/06/88	493.37	25.68	467.69		
	01/17/89	493.37	24.92	468.45		
	06/06/89	493.37	25.53	467.84		
	06/07/89	493.37	25.60	467.77		
	09/13/89	493.37	25.94	467.43		
	09/28/89	493.37	25.70	467.67		
	√11/10/89	493.37	27.10	466.27		
	01/29/90	493.37	27.16	466.21		
	01/30/90	493.37	27.18	466.19		
	01/31/90	493.37	27.23	466.14		
	02/01/90	493.37	27.26	466.11		
	02/02/90	493.37	27.24	466.13		
	02/09/90	493.37	27.30	466.07		
	02/22/90	493.37	26.40	466.97		
	03/01/90	493.37	25.96	467.41		
	03/13/90	493.37	25.79	467.58		
	04/03/90	493.37	23.58	469.79		
	04/12/90	493.37	24.17	469.20		
	07/18/90	493.37	22.56	470.81		
	10/11/90	493.37	24.26	469.11		

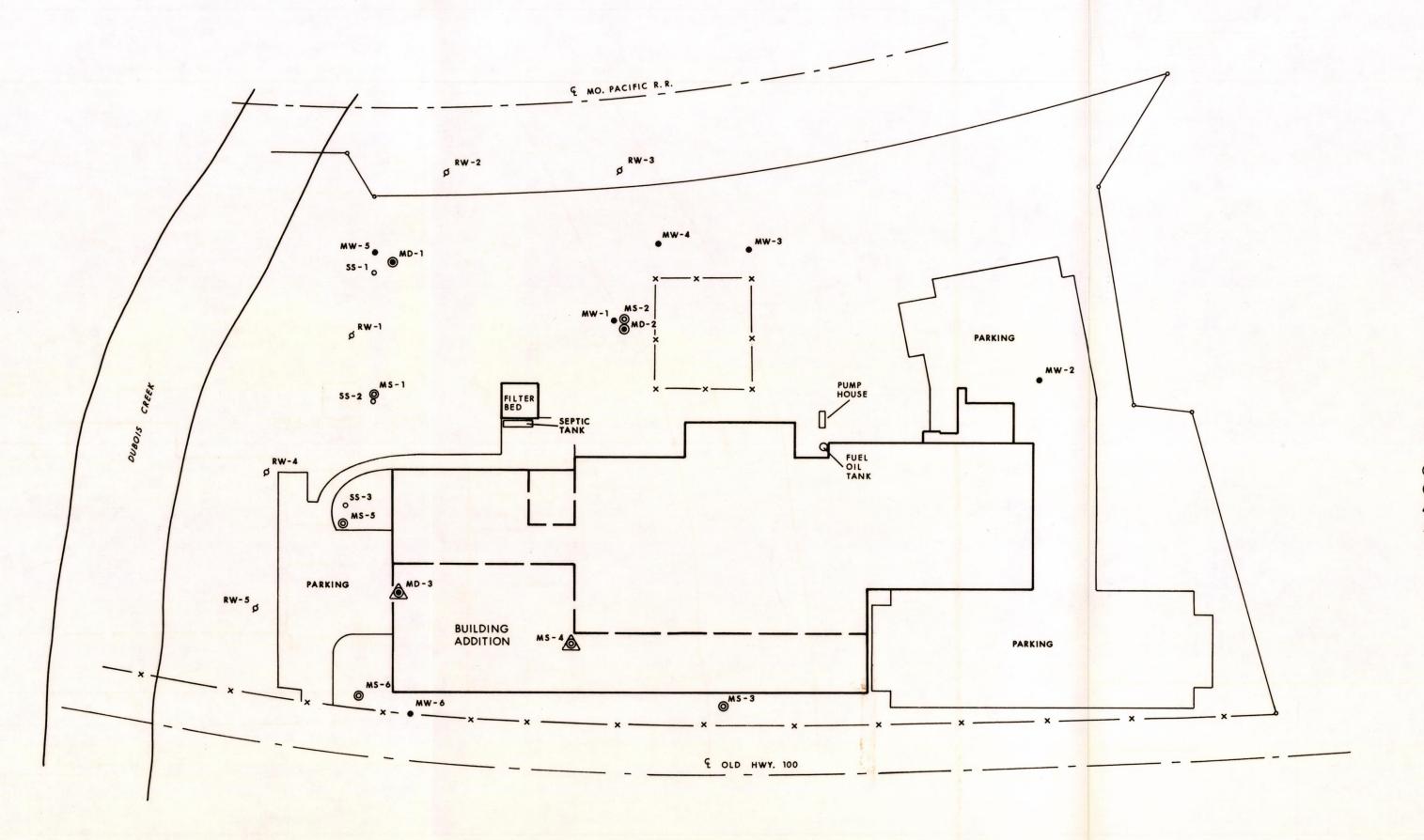
Well	Date	TOC Elev. (ft MSL)	Depth to Water (ft BTOC)	Water Elevation (ft. MSL)	Flow Rate (gpm)	Cumulative Flow (gallons)
DUBOIS WL	09/13/89	493.27	19.22	474.05		
	09/28/89	493.27	34.11	459.16		
	<i>-</i> 11/10/89	493.27	34.13	459.14		
	01/29/90	493.27	34.50	458.77		
	01/31/90	493.27	34.53	458.74		
	02/01/90	493.27	35.20	458.07		
	02/02/90	493.27	32.85	460.42		
	03/01/90	493.27	32.88	460.39		
	03/13/90	493.27	31.88	461.39		
	04/03/90	493.27	28.62	464.65		
	04/12/90	493.27	29.52	463.75		
	07/18/90	493.27	31.05	462.22		
	12/29/90	493.27	34.50	458.77		
	10/12/90			EST 460		

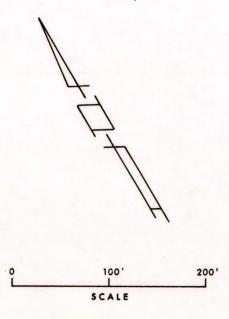
gpm	Gallons per minute
MSL	Mean sea level
TOC	Top of casing
BTOC	Below top of casing

Ground Water Recovery System Efficiency, SECO Products Facility, Washington, Missouri, Hussmann Corporation Table 4.

Compound	Influent	Effluent	Removal Efficiency
Acetone	28	35	*
Methylene Chloride	ND	6	*
1,1-Dichloroethene	14	ND	100
1,2-Dichloroethene	7,900	66	99
Trichloroethene	170	ND	100
Vinyl Chloride	170	ND	100

Common laboratory contaminant Not detected



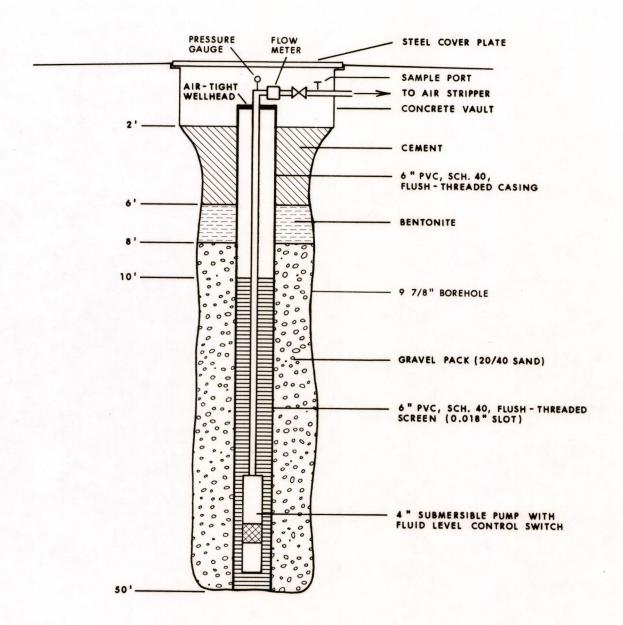


- ORIGINAL MONITOR WELL
- O SHALLOW MONITOR WELL
- MIDDLE MONITOR WELL
- DEEP MONITOR WELL
- PLUGGED MONITOR WELL
- of RECOVERY WELL

SECO PRODUCTS

SITE MAP



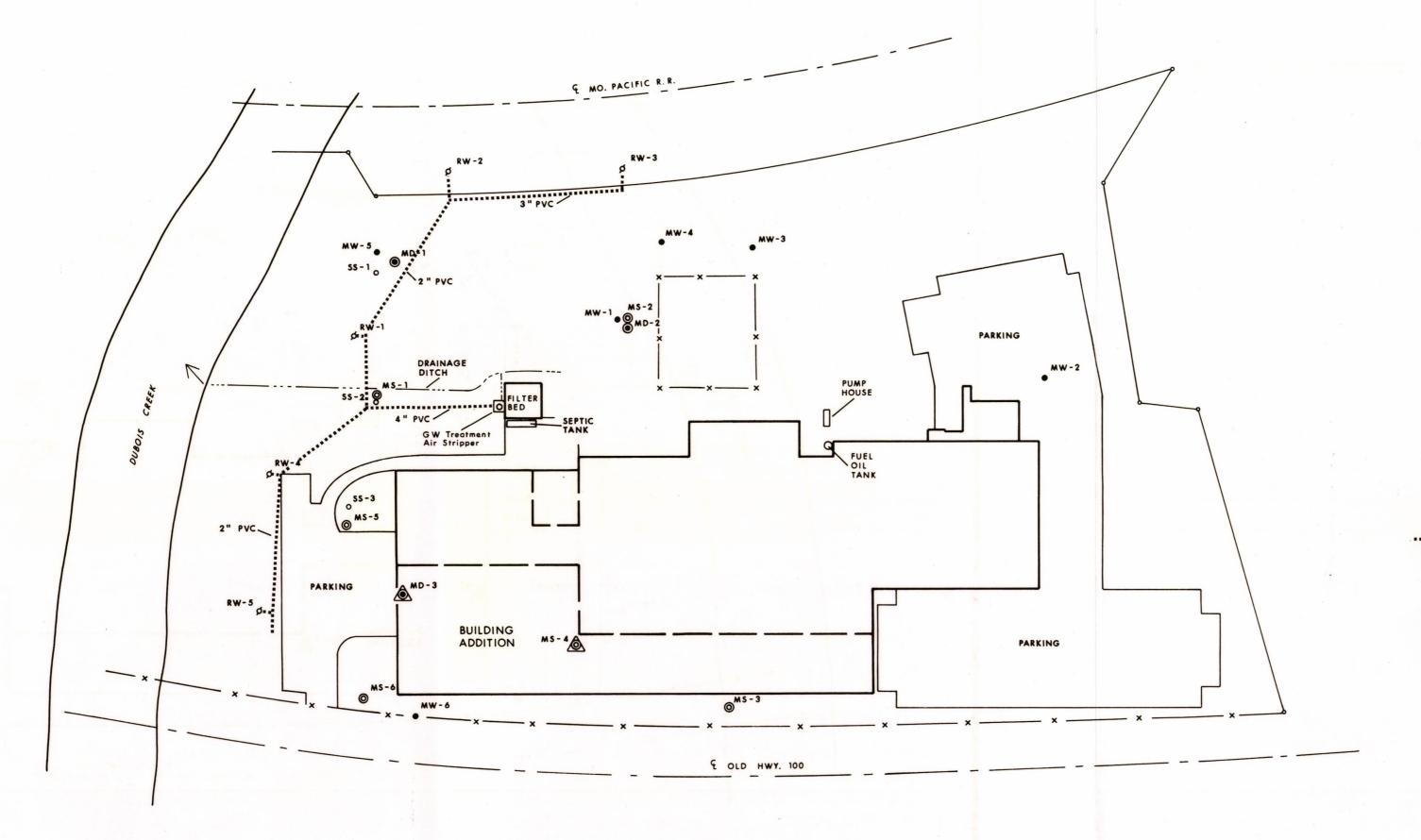


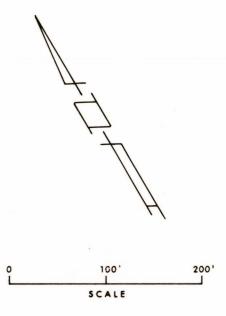
DRAWING NOT TO SCALE

SECO PRODUCTS

TYPICAL RECOVERY WELL DESIGN







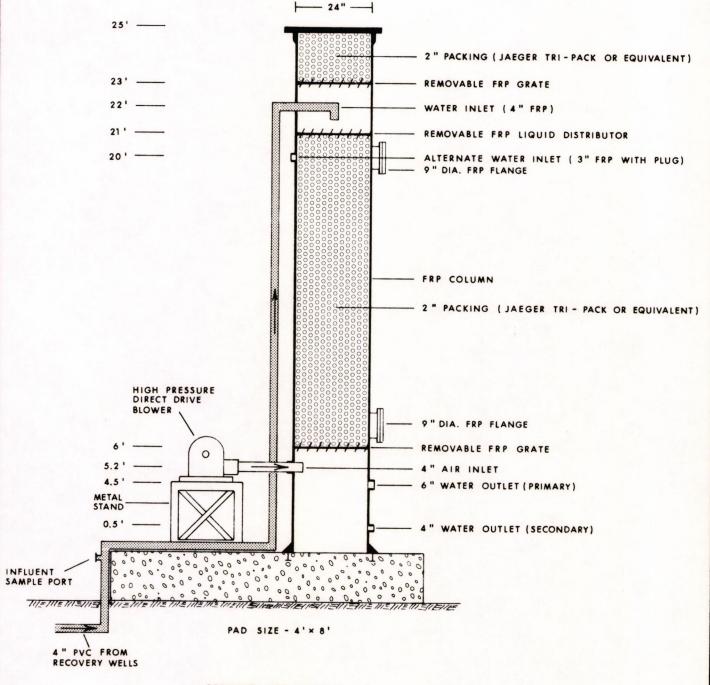
- ORIGINAL MONITOR WELL
- O SHALLOW MONITOR WELL
- MIDDLE MONITOR WELL
- DEEP MONITOR WELL
- A PLUGGED MONITOR WELL
- RECOVERY WELL

RECOVERY WELL PIPING

SECO PRODUCTS

GROUND WATER RECOVERY SYSTEM DESIGN



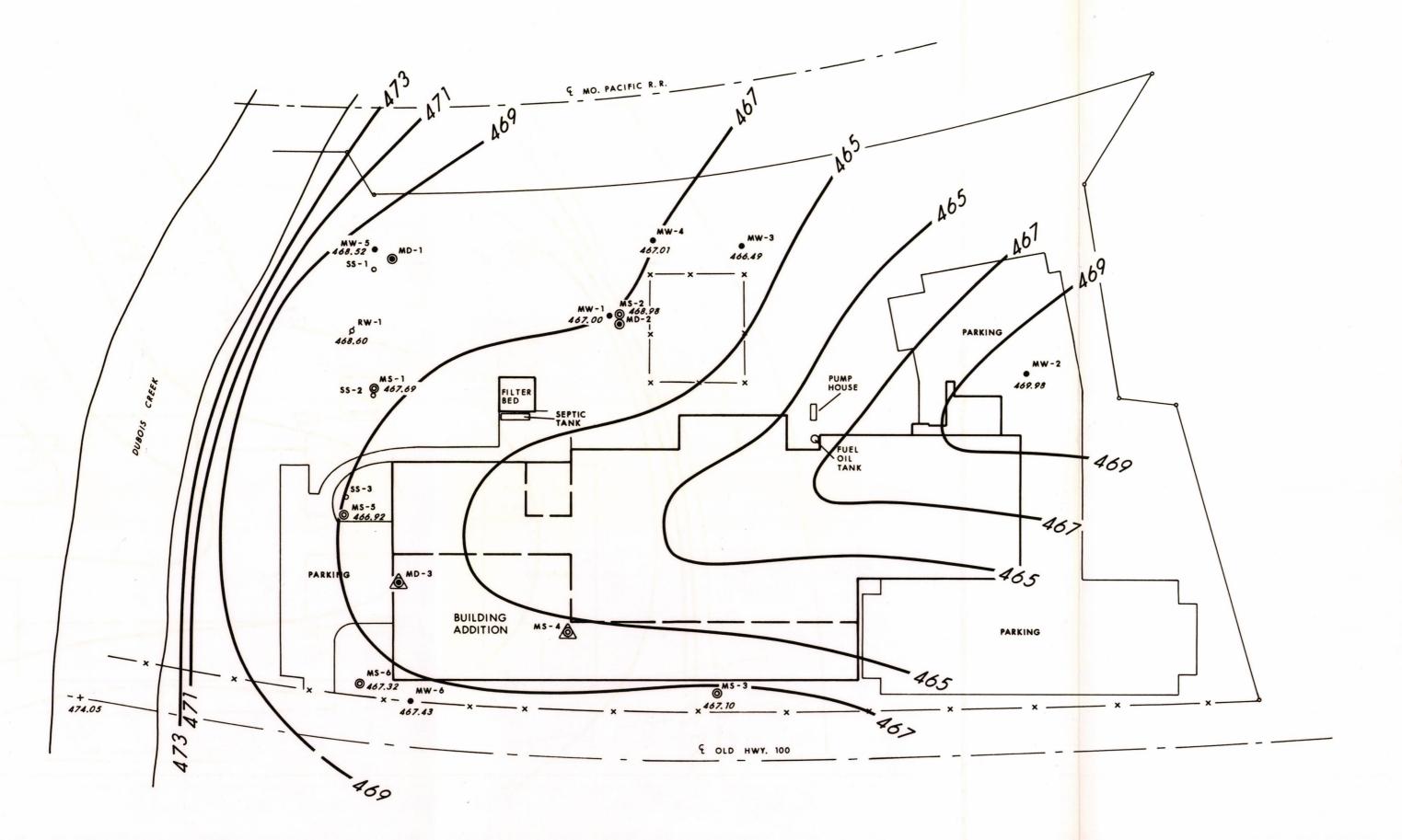


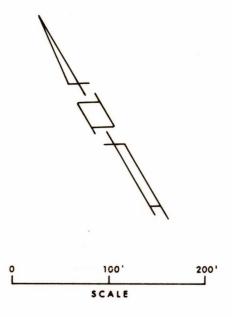
DRAWING NOT TO SCALE

SECO PRODUCTS

AIR STRIPPER DESIGN





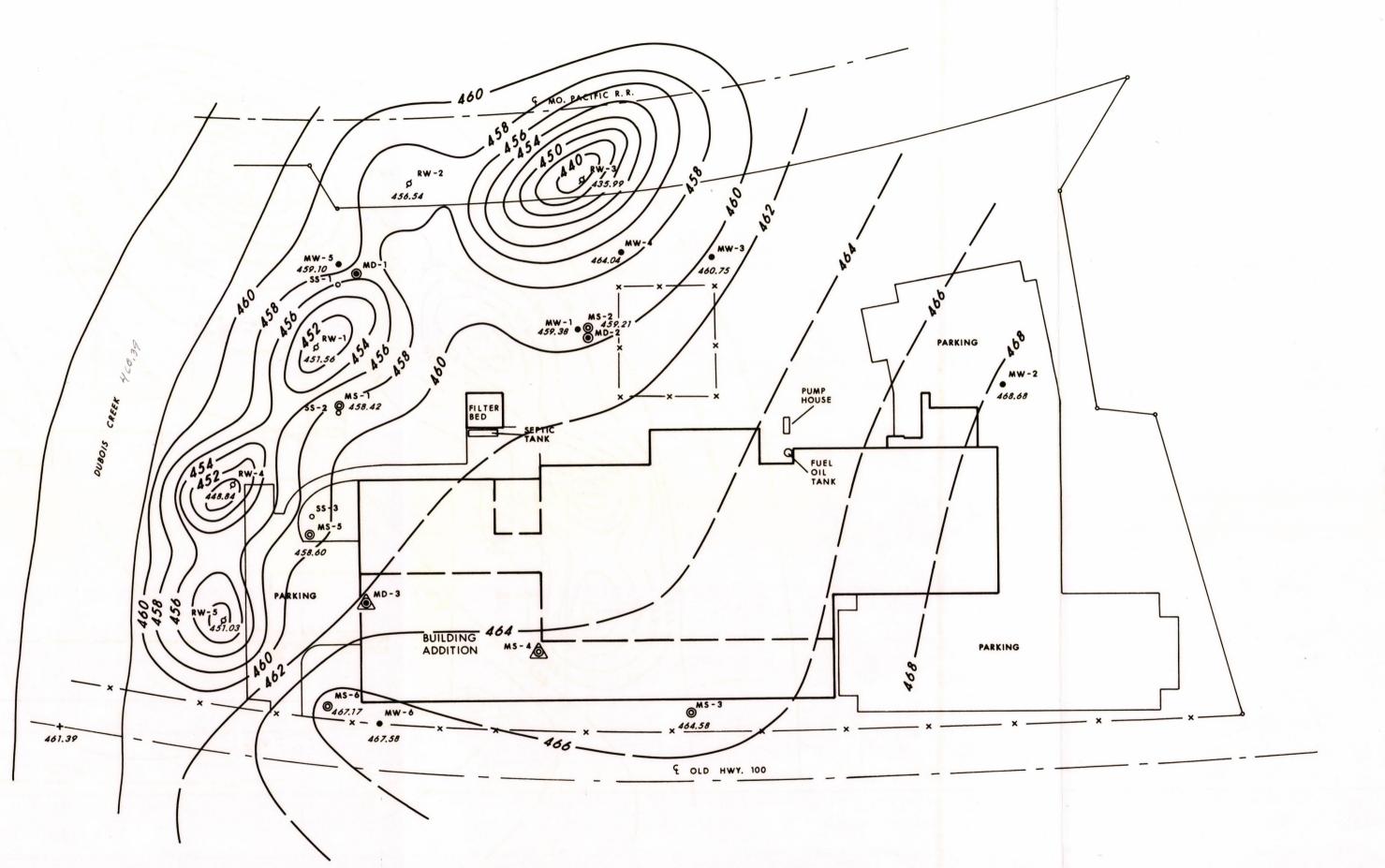


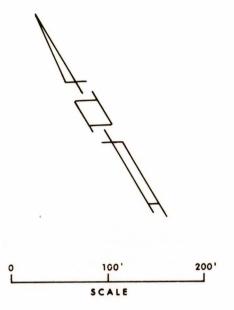
- ORIGINAL MONITOR WELL
- O SHALLOW MONITOR WELL
- MIDDLE MONITOR WELL
- DEEP MONITOR WELL
- A PLUGGED MONITOR WELL
- RECOVERY WELL

SECO PRODUCTS

MIDDLE SAND WATER TABLE HIGH STREAM STAGE SEPTEMBER 13, 1989







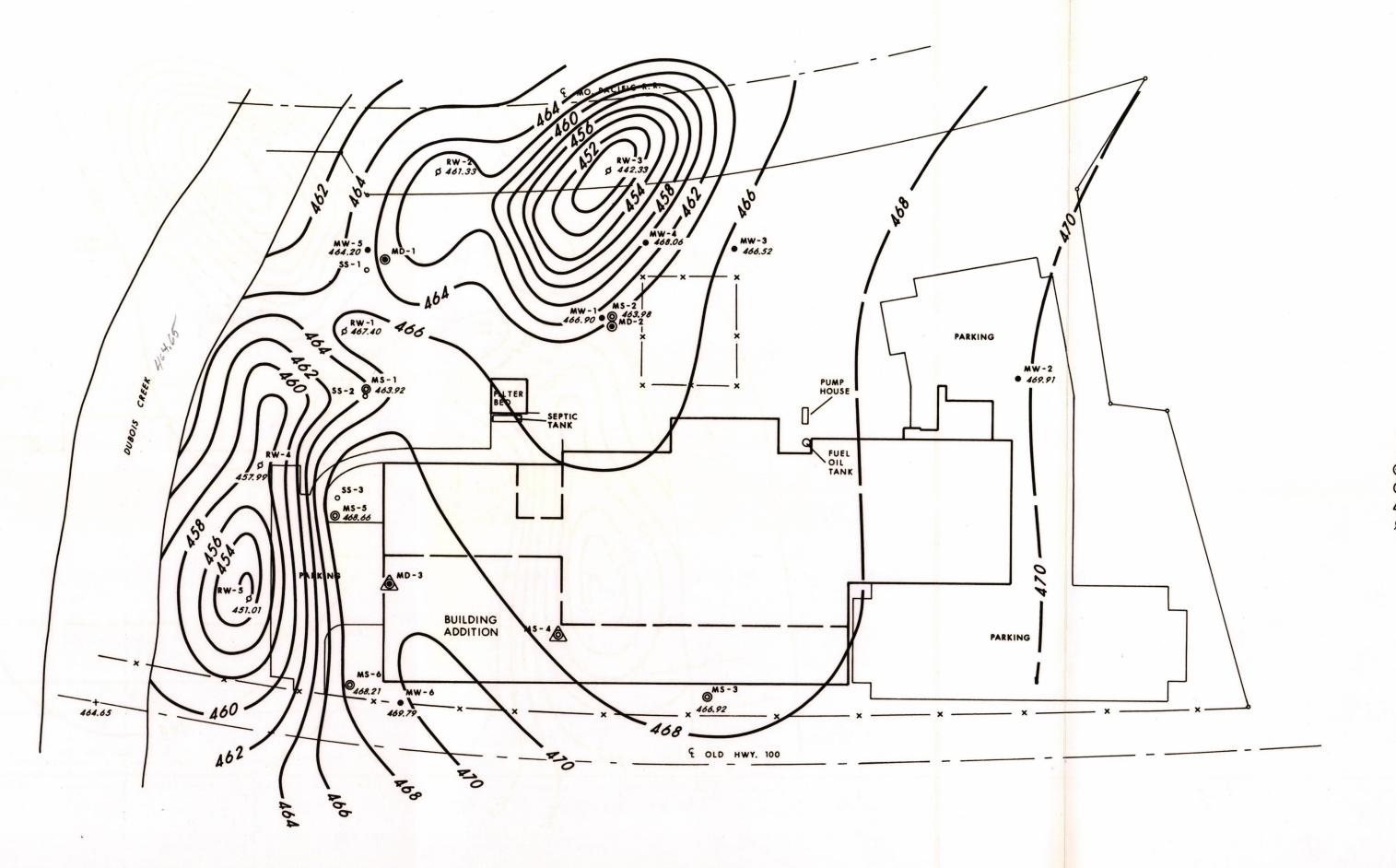
- ORIGINAL MONITOR WELL
- SHALLOW MONITOR WELL
- MIDDLE MONITOR WELL
- DEEP MONITOR WELL
- PLUGGED MONITOR WELL
- RECOVERY WELL

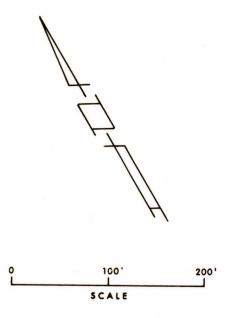
NOTE: SYSTEM FLOW RATE - 42 GPM

SECO PRODUCTS

PUMPING WATER TABLE MAP MARCH 13, 1990







- ORIGINAL MONITOR WELL
- O SHALLOW MONITOR WELL
- MIDDLE MONITOR WELL
- DEEP MONITOR WELL
- A PLUGGED MONITOR WELL
- RECOVERY WELL

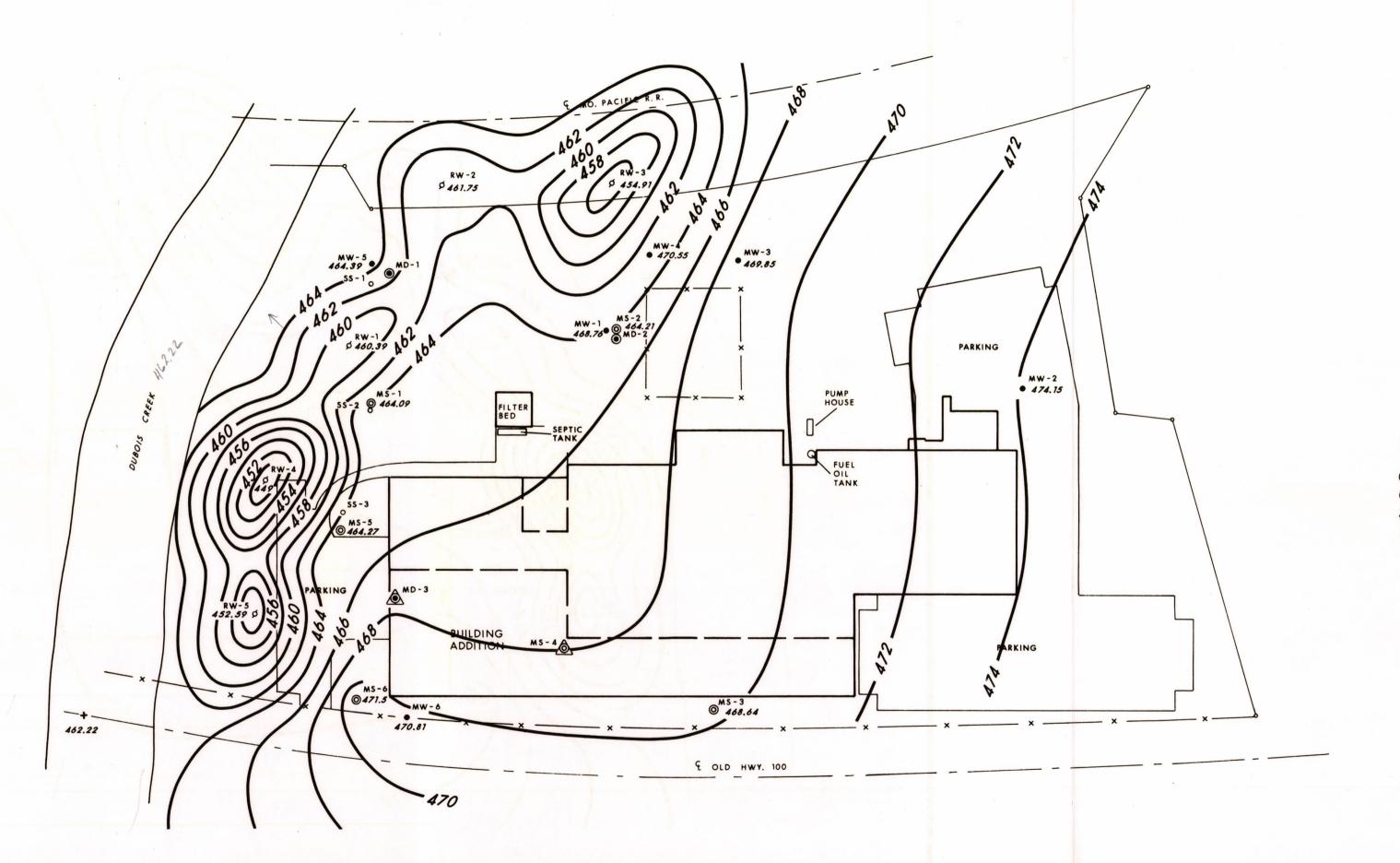
NOTE: SYSTEM FLOW RATE - 36 GPM

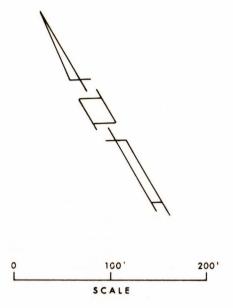
RECOVERY WELL RW - 1 SHUT DOWN
FOR MAINTENANCE

SECO PRODUCTS

PUMPING WATER TABLE MAP APRIL 3, 1990







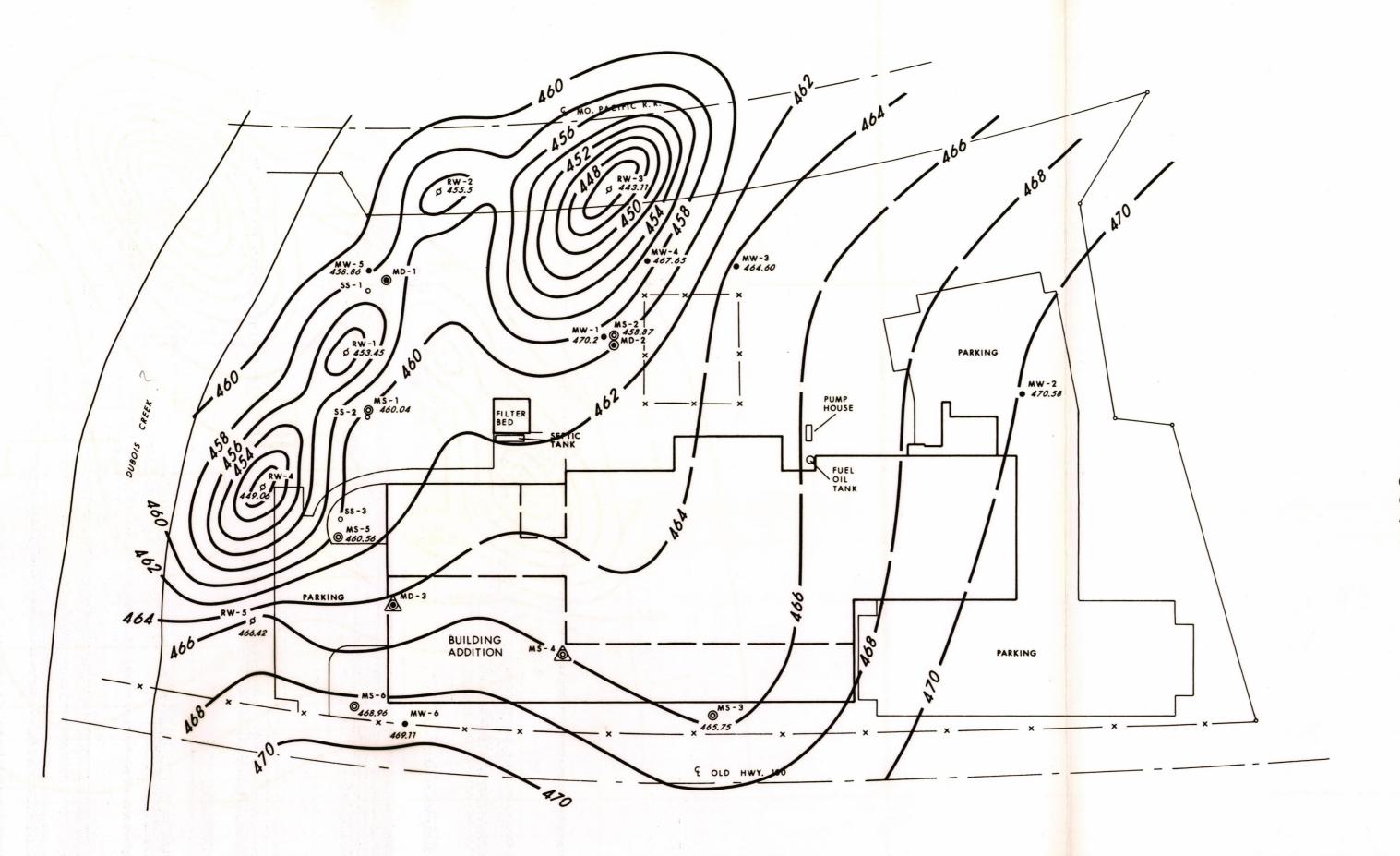
- ORIGINAL MONITOR WELL
- SHALLOW MONITOR WELL
- MIDDLE MONITOR WELL
- DEEP MONITOR WELL
- PLUGGED MONITOR WELL
- & RECOVERY WELL

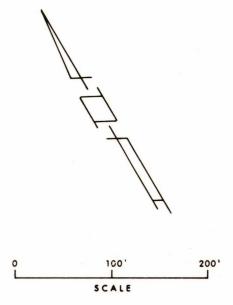
NOTE: SYSTEM FLOW RATE - 32 GPM

SECO PRODUCTS

PUMPING WATER TABLE MAP JULY 18, 1990







- ORIGINAL MONITOR WELL
- SHALLOW MONITOR WELL
- MIDDLE MONITOR WELL
- DEEP MONITOR WELL
- △ PLUGGED MONITOR WELL
- & RECOVERY WELL

NOTE: SYSTEM FLOW RATE - 35 GPM

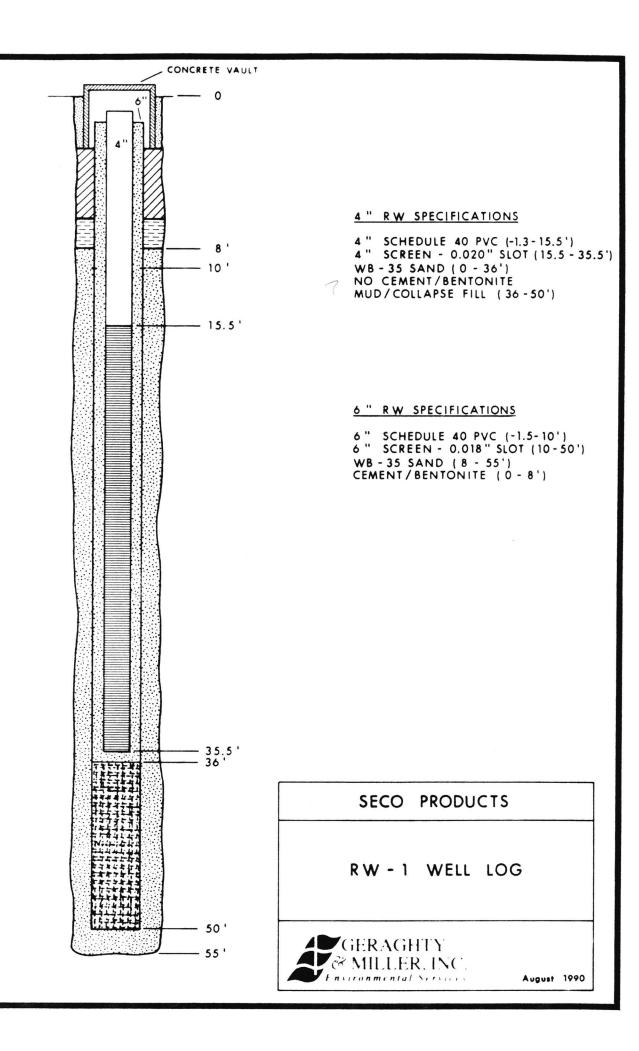
SECO PRODUCTS

PUMPING WATER TABLE MAP OCTOBER 12, 1990



APPENDIX A

BORING LOGS AND WELL COMPLETION DIAGRAMS



Hussmann

PROJECT

LOCATION

Hussmann-SECO

Washington, Missouri

WELL LOG

ELEVATION Ground Level Casing

Water Level

CASING

6" Sch. 40 PVC (+3-10')

COMPLETION

6" screen (0.018" slot) (10-50') WB-35 sand (8-55')

Cement-bentonite (0-8')

CEMENT WELL NO. RW-1 LITHOLOGY COMPLETION I DEPTI 80 HOLE GEOPHYSICAL LOG SAMPLE LOG SYM SIZE n-n-n Dk. brown, silty clay (cl); med. stiff; moist; 10-20% silt חבחב תבת _ ד_ דר 5 חר_חר. 10- H H H Dk. brown, silty sand (sm); med. 10 dense; moist; v. fine sand; II. H 30-40% silt. dt :: 44 - 41 14. 14 11 11 11 15-15 Becomes saturated at 15 feet. Dk. brown, silty clay (cl); med. stiff; moist; 15-25% silt. Dk. brown, sandy clay (cl); med. stiff; moist; 25-35% v. fine sandy; 5-15% silt. 20-**-** 20 Dk. gray, silty sand (sm); med. n n dense; saturated; v. fine - 11 sand; 35-45% silt. D 11 Less silt at 23 feet (10-20%). Dk. gray, sandy clay (cl); med. 25-- 25 stiff; moist; 20-30% v. fine sand. 11 11 11 Dk. gray, silty sand (sm); med. n n dense; saturated; v. fine sand; 10-20% silt.



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BENTONITE SEAL

PUMP SETTING

GRAVEL PACK

CEMENT

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PERFORATIONS



Dk. gray, silty clay (cl); med.

Dk. gray, silty sand (sm); med. dense; saturated; v. fine

stiff; moist; 25-35% silt.

sand; 5-15% silt.

REED & ASSOCIATES, INC.

30

Hydrologists and Environmental Consultants AUSTIN . CORPUS CHRISTI . MIDLAND

Hussmann

PROJECT Hussmann-SECO

LOCATION

WELL NO.

Washington, Missouri

_RW-1

WELL LOG

ELEVATION

Ground Level

Casing

Water Level

CASING

6" Sch. 40 PVC (+3-10')

COMPLETION

6" PVC screen (0.018" slot) (10-50') WB-35 sand (8-55')

CEMENT

Cement-bentonite (0-8')

				ment-bentonite		
1 -		LITHOLOGY			COMPLETION	
DEPTH	SYMBOL	GEOPHYSICAL LOG	SAMPLE LOG		HOLE SIZE	DEPTH
40 - 45 - 60 - 65 - 65 - 65 - 65 - 65 - 65 - 6			<pre>Dk. gray, silty clay (cl); med stiff; moist; 15-25% silt. Dk. gray, silty sand (sm); med dense; saturated; v. fine sand; 5-15% silt. Dk. gray, silty clay (cl); med stiff; moist; 10-20% silt. Total depth is 55 feet.</pre>		9 3/4	45



WATER LEVEL

PUMP SETTING



CEMENT



BENTONITE SEAL



GRAVEL PACK



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Hussmann Corporation CLIENT

PROJECT Hussmann SECO

LOCATION

Washington, Missouri

WELL NO.

RW-2

WELL LOG

ELEVATION Ground Level Casing Water Level CASING

6" PVC, Sch. 40 (-1-15') 6" PVC, 0.018" slot (15-75')

COMPLETION CEMENT

WB-25 sand (10-76') Cement-bentonite (0-10')

	_		ment-bentonit		
-		LITHOLOGY		COMPLETION	
DEPTH	SYMBOL	SAMPLE LOG	,	HOLE SIZE	DEPTH
5		Dark brown, silty clay (cl); medium stiff, moist; 30 to 40% silt.		9 7/8 ⁿ	5
10		<pre>Dark brown, sandy clay (cl); medium stiff, moist; 30 to 40% very fine sand; ≤2 to 7% silt. Dark brown, clayey sand (sc); medium dense; very fine sand; 30 to 40% clay; ≤5 to 15% silt.</pre>			10
15 -		Dark brown, silty clay (cl); medium stiff; moist; 30 to 40% silt.	; 		15
20 -		Change in color at 19 feet to dark gray. Dark gray, clayey sand (sc); medium dense; very fine sand; 25 to 35% clay; 10 to 20% silt. Dark gray, silty clay (cl); medium stiff; moist; 30 to 40% silt. Dark gray, silty sand (sm); medium dense; very			20
25	V 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	fine sand; 30 to 40% silt. Dark gray, silty clay (cl); medium stiff; moist; 30 to 40% silt. Dark gray, clayey sand (sc); medium dense; very fine sand; 20 to 30% clay; 5 to 15% silt. Dark gray to black, gravelly sand (sp); med.			25
30		dense; subrounded to subangular, medium to very coarse sand; subangular gravel to 3/16" diameter. Dark gray to black, sandy gravel (gp); medium dense, subrounded gravel to 1/2" diameter; 25 to 35% coarse to very coarse sand.			30

WATER LEVEL

PUMP SETTING

CEMENT

BENTONITE SEAL

GRAVEL PACK

PERFORATIONS



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<u>Hussmann Corporation</u>

Washington, Missouri

PROJECT

LOCATION

Hussmann SECO

WELL LOG

ELEVATION Ground Level

Casing

Water Level CASING

6" PVC, Sch. 40 (-1-15')

6" PVC, 0.018" slot (15-75')

COMPLETION

WB-25 sand (10-76') RW-2WELL NO. CEMENT Cement-bentonite (0-10') LITHOLOGY COMPLETION DEPTH SYMBO HOLE SAMPLE LOG SIZE 9 7/8" 40 40 45 45 50 50 Dark gray sand (sp); medium dense; very fine to fine sand. 55 -55 Minor silt and clay at 59 feet. Gray, sandy gravel (gp); medium dense to dense; subrounded gravel to 1" diameter; 20 to 30% very fine to very coarse, subrounded to 60 -60 subangular sand; ≤2 to 7% clay. Dark gray, silty sand (sm); medium dense; very fine to fine sand; 30 to 40% silt. 65 -65 Minor clay from 66 to 67 feet (5 to 10%). Two-inch to three-inch interbedded, sandy

WATER LEVEL

BENTONITE SEAL

clay layers from 69 to 73 feet.

PUMP SETTING

GRAVEL PACK

CEMENT

PERFORATIONS



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PROJECT

Hussmann SECO

WELL LOG

ELEVATION Ground Level

Casing Water Level

COMPLETION

CASING

6" PVC, Sch. 40 (-1-15') 6" PVC, 0.018" slot (15-75')

WB-25 sand (10-76')

Cement-bentonite (0-10')

Washington, Missouri LOCATION

WELL NO.

RW-2

CEMENT LITHOLOGY COMPLETION DEPTH DEPTH SYMBOI HOLE SAMPLE LOG SIZE 9 7/8" 10 to 15% medium to coarse sand interspersed from 73 to 74 feet. Dark gray, silty clay (cl); stiff to very stiff; moist; 15 to 25% silt. 75 75 1" Core Sample Total depth is 78 feet. 80 80 85 85 90 90 95 95 100--100



PUMP SETTING

CEMENT



BENTONITE SEAL



GRAVEL PACK



PERFORATIONS



REED & ASSOCIATES, INC.

Hydrologists and Environmental Consultants AUSTIN . CORPUS CHRISTI . MIDLAND

Hussmann Corporation

PROJECT

Hussmann SECO

WELL LOG

ELEVATION Ground Level

Casing Water Level

CASING

6" PVC, Sch. 40 (-1-17') 6" PVC, 0.018" slot (17-67')

WB-25 sand (12-69')

COMPLETION

Washington, Missouri LOCATION

WELL	NO.	RW-3 CEMENT CE	ment-bentonit	e (0-12')	
_	LITHOLOGY		COMPLETION		
DEPTH	SYMBOL	SAMPLE LOG		HOLE SIZE	DEPTH
5		Dark brown, silty clay (cl); medium stiff; moist; 25 to 35% silt.		9 7/8"	5
10 -		Dark brown, sandy clay (cl); medium stiff; moist; 20 to 30% very fine sand; ≤2 to 10% silt. Dark brown, silty sand (sm); medium dense; very fine sand; 30 to 40% silt.			-10
15					-15 -
20 -		Dark gray, silty clay (cl); medium stiff; moist; 25 to 35% silt. Dark gray, silty sand (sm); medium dense; very fine sand; 30 to 40% silt.			- - - 20
25		Less silt at 22 feet (15 to 25%).			- - - 25 - -
30 -					30
=		Becomes siltier at 33 feet (25 to 35% silt).			

WATER LEVEL

BENTONITE SEAL

PUMP SETTING

GRAVEL PACK

CEMENT

PERFORATIONS



REED & ASSOCIATES, INC.

Hydrologists and Environmental Consultants
AUSTIN • CORPUS CHRISTI • MIDLAND

Hussmann Corporation

PROJECT

Hussmann SECO

WELL Ground Level
Casing
Water Level
CASING

Casing
Water Level
SING
6" PVC, Sch. 40 (-1-17')

LOCATION

Washington, Missouri

COMPLETION

ELEVATION

6" PVC, 0.018" slot (17-67') WB-25 sand (12-69')

ELL NO. RW-3

WELL	NO.	RW-3 CEMENT CE	ment-bentonit	e (0-10')	
_	LITHOLOGY			TION	
DEPTH	SYMBOL	SAMPLE LOG		HOLE SIZE	DEPTH
		Dark gray, clayey sand (sc); medium dense; very fine sand; 20 to 30% clay.		9 7/8"	
40		Less clay at 41 feet (10 to 20%).			40
45		Brown and black sand (sp); medium dense to dense fine to very coarse grain, subrounded sand.	;		
50		Sand becomes very fine to fine at 54 feet.			50
55					- - - - - - - - - - - -
60		Dark gray, silty sand (sm); medium dense; very fine to fine sand; 15 to 25% silt.			60
65		<pre>Brown and black sand (sp); medium dense to dense medium to very coarse, subrounded to subangular sand. Dark gray, silty sand (sm); medium dense; very fine sand; 20 to 30% silt.</pre>			- - - - - 65
-		Dark gray, silty clay (cl); medium stiff; moist; 30 to 40% silt; small very fine sand pockets. Total depth is 70 feet.			

▼ WATER LEVEL

BENTONITE SEAL

--- PUMP SETTING

GRAVEL PACK

CEMENT

PERFORATIONS



REED & ASSOCIATES, INC.

Hydrologists and Environmental Consultants
AUSTIN • CORPUS CHRISTI • MIDLAND

Hussmann Corporation CLIENT

PROJECT

WELL Hussmann SECO LOG

Ground Level Casing Water Level CASING

ELEVATION

6" PVC, Sch. 40 (-1-13')

COMPLETION

6" PVC, 0.018" slot (13-43') WB-25 sand (10-45')

Washington, Missouri LOCATION

WELL NO. RW-4CEMENT Cement-bentonite (0-10') LITHOLOGY COMPLETION DEPTH SYMBOI HOLE SAMPLE LOG SIZE 9 7/8" Dark brown, silty clay (cl); medium stiff; moist; 20 to 30% silt. 5 Brown, silty sand (sm); medium dense; moist, very fine sand; 30 to 40% silt; ≤2 to 5% clay; limonitic staining. 10 -10 15 -15 Becomes clayier at 17 feet (5 to 15%). Dark gray, sandy silt/silty sand (ML/SM); medium stiff; very fine sand; ≤2 to 5% clay. 20 -20 Dark gray, silty sand (sm); medium stiff; very fine sand; 35 to 45% silt. 25 -25 30 -30 Less silt at 34 feet (25 to 35%).

WATER LEVEL

BENTONITE SEAL

PUMP SETTING

GRAVEL PACK

CEMENT

PERFORATIONS



REED & ASSOCIATES, INC.

Hydrologists and Environmental Consultants AUSTIN . CORPUS CHRISTI . MIDLAND

Hussmann Corporation

PROJECT

Hussmann SECO

LOCATION

Washington, Missouri

WELL LOG

ELEVATION Ground Level Casing Water Level CASING

6" PVC, Sch. 40 (-1-13') 6" PVC, 0.018" slot (13-43')

COMPLETION CEMENT

WB-25 sand (10-45')

WELL N	10. <u>I</u>	RW-4 CEMENT		3-25 sand (10- ement-bentonit		
_	LITHOLOGY			COMPLE	TION	
DEPTH	SYMBOL	SAMPLE LOG			HOLE SIZE	DEPTH
40 45 50 55 60 65		Sand becomes very fine to fine at 36 feet; silt (15 to 25%). Dark gray, clayey sand (sc); medium dense; fine sand; 15 to 25% clay; ≤5 to 15% silt Dark gray, silty clay (cl); medium stiff to moist; 20 to 30% silt. Total depth is 45 feet.	very t.	f;	9 7/8"	40

WATER LEVEL

PUMP SETTING

CEMENT

BENTONITE SEAL



GRAVEL PACK



PERFORATIONS



REED & ASSOCIATES, INC.

Hydrologists and Environmental Consultants
AUSTIN • CORPUS CHRISTI • MIDLAND

Hussmann Corporation

Washington, Missouri

PROJECT

LOCATION

Hussmann SECO

WELL LOG

ELEVATION Ground Level Casing

Water Level CASING

6" PVC, Sch. 40 (-1-13') 6" PVC, 0.018" slot (13-48')

WB-25 sand (10-48')

COMPLETION

WELL NO. RW-5CEMENT Cement-bentonite (0-10') LITHOLOGY COMPLETION DEPT DEPTH SYMBO HOLE SAMPLE LOG SIZE 9 7/8" Brown, silty sand (sm); medium dense; moist; very fine sand; 30 to 40% silt. 5 5 Brown and gray mottled, sandy clay (cl); medium stiff; moist; 25 to 35% very fine sand; 10 to 20% silt; limonitic staining. Dark brown, silty sand (sm); medium dense; very 10 10 fine sand; 30 to 40% silt; ≤2 to 7% clay. Brown, silty clay (cl); medium stiff; moist; 20 to 30% silt; limonitic staining. Dark brown, silty sand (sm); medium dense; very 15 15 fine sand; 30 to 40% silt. Brown, silty clay (cl); medium stiff; moist; 25 to 35% silt; limonitic staining. Dark gray, silty sand (sm); medium dense; very fine sand; 30 to 40% silt; ≤2 to 7% clay. 20 20 5 to 15% medium to course grain sand from 20 to 22 Dark gray, sandy silt (ml); medium stiff; moist; 25 to 35% very fine sand; ≤2 to 5% clay. Dark gray, silty clay (cl); medium stiff; moist; 25 25 20 to 30% silt. Minor sand and silt interbeds from 28 to 30 feet. 30 30 10 to 20% very fine sand from 33 to 34 feet.

WATER LEVEL

<u>|---</u> BENTONITE SEAL

PUMP SETTING

GRAVEL PACK

CEMENT

PERFORATIONS



REED & ASSOCIATES, INC.

Hydrologists and Environmental Consultants AUSTIN . CORPUS CHRISTI . MIDLAND

Hussmann Corporation

Washington, Missouri

PROJECT

LOCATION

Hussmann SECO

WELL LOG ELEVATION

Ground Level
Casing
Water Level

CASING 6" PVC, Sch. 40 (-1-13')

COMPLETION

6" PVC, 0.018" slot (13-48') WB-25 sand (10-48')

RW-5WELL NO. CEMENT Cement-bentonite (0-10') LITHOLOGY COMPLETION I DEPT SYMBOI HOLE SAMPLE LOG SIZE 9 7/8" 40 40 Dark gray, sandy silt/silty sand (ml/sm); medium stiff; moist; very fine sand; ≤2 to 5% 45 45 clay. Dark gray, silty clay (cl); medium stiff; moist; 30 to 40% silt. Dark gray, sandy silt/silty sand (ml/sm); medium stiff; moist; very fine sand. 1" Dark gray, silty clay (cl); medium stiff; moist; 50 50 25 to 35% silt. Total depth is 50 feet. 55 55 60 60 65 65

▼ WATER LEVEL

BENTONITE SEAL

--- PUMP SETTING

GRAVEL PACK

CEMENT

PERFORATIONS



REED & ASSOCIATES, INC.

Hydrologists and Environmental Consultants
AUSTIN • CORPUS CHRISTI • MIDLAND

APPENDIX B

GROUND WATER RECOVERY SYSTEM OPERATION AND MAINTENANCE PROCEDURES

APPENDIX B

HUSSMANN SECO GROUND WATER RECOVERY SYSTEM OPERATIONAL AND MAINTENANCE PROCEDURES

- Monitoring and Record Keeping
 - Daily monitoring and record keeping of the ground water recovery system will be performed by SECO Products personnel. The specific tasks to be performed daily including the following.
 - Record time of inspection
 - Record air stripper effluent discharge rate
 - Record total gallons discharged
 - Record in-line pressure
 - Inspect air stripper tower and blower

This data will be recorded on the Treatment Unit Inspection Log presented as Attachment 1.

- Quarterly inspections of the ground water treatment unit, including the five recovery wells, will be performed by G&M St. Louis personnel. The specific tasks to be performed during the quarterly inspection include the following.
 - Record time and date of inspection
 - Record if pump is on or off
 - Record total gallons discharged
 - Record pumping rate
 - Record in-line pressure
 - Record condition of well and piping
 - List any repairs or replacement of parts
 - Record time well out of service for repairs

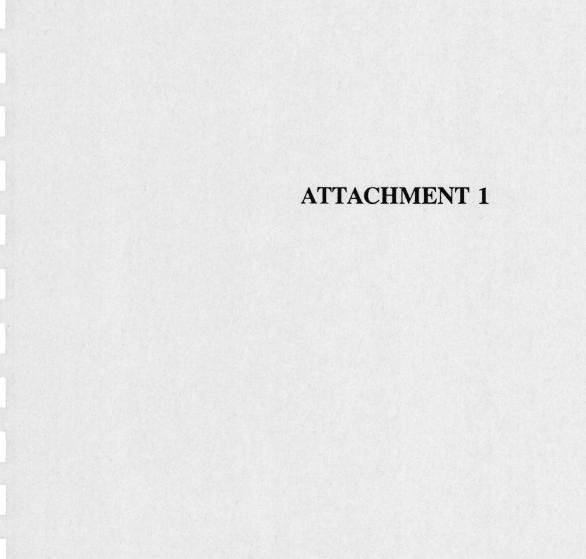
This data will be recorded on the Recovery Well Inspection Log presented as Attachment 2.

- System Failures and Reporting
 - A constant-flow rate should be maintained in each recovery well. The combined flow rate of each recovery well should total the air stripper effluent discharge flow rate which is recorded on a daily basis by SECO Products personnel. Should the effluent discharge flow rate fall by more than five gallons per minute, the following procedures should be performed.
 - Check each recovery well and note which well(s) is malfunctioning. If a recovery well is not operating, check the breaker at the control box. If the well(s) cannot be restarted by flipping the breaker switch, then the following people should be informed within 24 hours.
 - G&M St. Louis: (314) 569-0989

Mr. Tom Lazarski Mr. Douglas Marian

Hussmann Corporation: (314) 344-0541

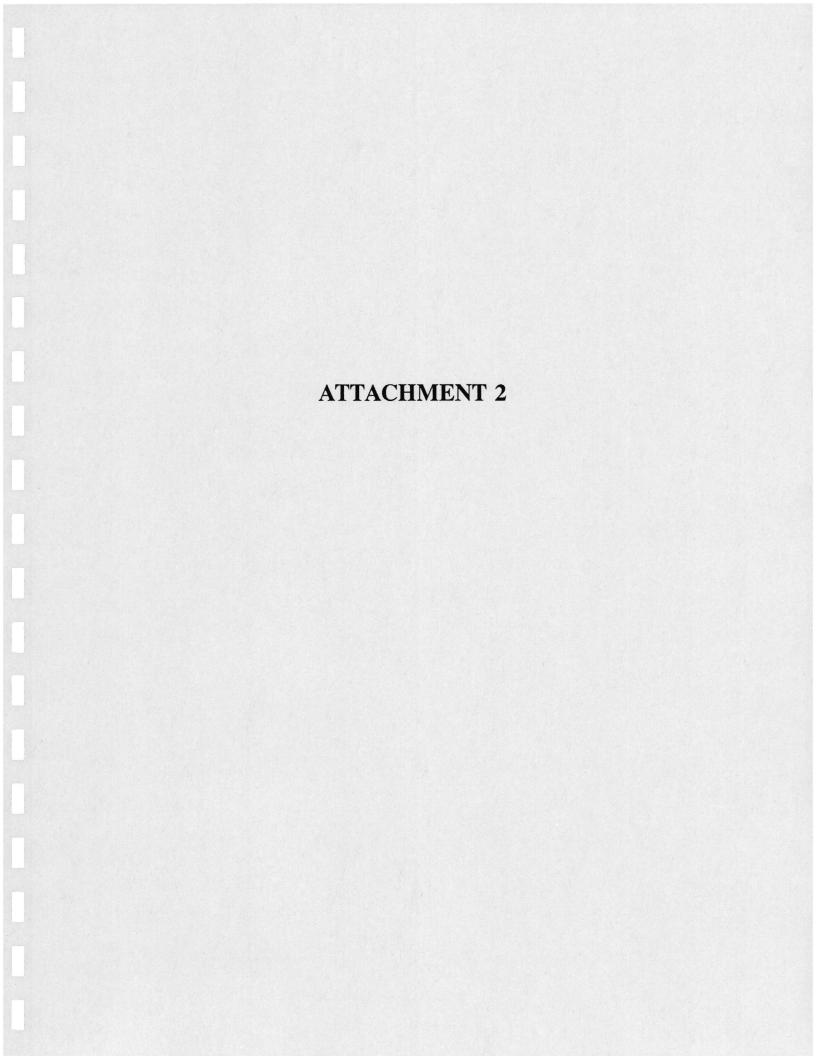
Mr. Dennis Dubitsky



HUSSMANN SECO TREATMENT UNIT INSPECTION LOG

Daily Inspection Log Month and Year

Day	Time	Flow Meter Reading	Gallons Discharged	Water Pressure (psi)	Air Stripper Blower On/Off	Air Stripper Condition	Inspector
1							
2							
3							
4							
5							
6							
7						9	
8							
9							
10							
11							
12							
13							
14							
15							
16		-					
17							
18							
19			V-145				
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27							
28			7777 - Ye 1841 - Ye				
29							
30							
31							



HUSSMANN SECO RECOVERY WELL INSPECTION LOG

Quarterly Inspection Log Recovery Well:	Month and Year:

Well	Time	Pump On/Off	Water Meter Reading	Gallons Discharged	Condition	Repairs, if any	Time Out Of Service	Inspector

			7					

						,		

				378/44A				

APPENDIX C

TREATMENT UNIT INSPECTION LOGS - 1990

HUSSM' SECO TREATMENT UN SPECTION LOG

Daily Inspectic. Log Month and Year March 1990

$\begin{array}{cccccccccccccccccccccccccccccccccccc$			7		7		(
2 0948 40 1,719,570 22 00 0V	Day					Air Stripper Blower On/Off	Air Stripper Condition	Inspector
2 0948 40 1,719,590 22 0N 0 LC 3	1		35	1,658,330	18	ОИ	OK	hc
3	2	0948	40		22	40		
5 0756 43 1,897,690 24 00 0K Lc 6 1255 43 1,970,920 25 00 0K Lc 7 1228 41 2,031,240 21 00 0K Lc 8 1400 43 2,031,240 21 00 0K Lc 9 1252 44 2,031,250 21 00 0K Lc 10 10 11 00 0K Lc 11 2,153,870 24 00 0K Lc 13 0700 42 2,380,739 24 00 0K Lc 13 0700 42 2,380,739 24 00 0K Lc 14 1600 40 2,461,780 23 00 0K Lc 15 0600 41 2,496,840 24 00 0K Lc 16 0700 37 2,720,819 20 00 0K Lc 20 0830 3	3							
6	4							
8	5	0756	43	1,897,690	24	60	OIC	1.0
7 1228 41 2,031,240 21 00 0K LC 8 1400 43 2,095,510 21 00 0K LC 9 1252 44 2,153,870 24 0N 0K LC 10 11 12 0721 42 2,322,560 25 00 0K LC 13 0700 42 2,380,739 24 00 0K LC 14 1600 40 2,461,780 23 00 0K LC 15 0600 41 2,496,840 24 00 0K LC 16 0700 38 2,558,340 21 00 0K LC 17 18 19 0700 37 2,720,819 20 00 0K LC 20 0830 39 2,777,245 19 00 0K LC 21 0900 37 2,836,456 20 00 0K LC 22 0700 37 2,836,456 20 00 0K LC 23 1030 38 2,918,821 18 00 0K LC 24 25 26 1030 38 3,080,864 19 00 0K LC 25 26 1030 38 3,179,467 20 00 0K LC 26 0630 37 3,233,857 18 00 0K LC 29 0700 37 3,233,857 18 00 0K LC 29 0700 37 3,233,857 18 00 0K LC 29 0700 37 3,233,857 18 00 0K LC 20 0800 37 3,289,222 19 00 0K LC 20 0800 37 3,289,222 19 00 0K CC 21 0700	6	1255	43	,	25	00		
8	7	1228	41		21			
9 1252 44 2,153,810 24 ON OK LC 10 11 12 0721 42 2,322,560 25 ON OK LC 13 0700 42 2,380,739 24 ON OK LC 14 1600 40 2,461,780 23 ON OK LC 15 0600 41 2,496,840 24 ON OK LC 16 0700 38 2,558,340 21 ON OK LC 17 18 19 0700 37 2,720,819 20 ON OK LC 20 0830 39 2,777,245 19 ON OK LC 21 0900 37 2,836,456 20 ON OK LC 22 0700 37 2,836,456 20 ON OK LC 23 1030 38 2,918,821 18 ON OK LC 24 25 26 1030 38 3,080,864 19 ON OK LC 27 0700 37 3,127,579 19 ON OK LC 28 0630 38 3,179,467 20 ON OK LC 29 0700 37 3,233,857 18 ON OK LC 29 0700 37 3,233,857 18 ON OK LC 29 0700 37 3,289,222 19 ON OK LC	8	1400	43	2.095,510				
10 11 12 12 13 14 14 15 15 16 16 17 18 19 19 19 19 19 19 19 19 19 19 19 19 19	9	1252	44		24			
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13 0700 42 2,380,739 24 0N 0K LC 14 1600 40 2,461,780 23 0N 0K LC 15 0600 41 2,496,840 24 0N 0K LC 16 0700 38 2,558,340 21 0N 0K LC 17 18 19 0700 37 2,720,819 20 0N 0K LC 20 0830 39 2,777,245 19 0N 0K LC 21 0900 37 2,836,456 20 0N 0K LC 22 0700 37 2,836,456 20 0N 0K LC 23 1030 38 2,918,821 18 0N 0K LC 24 25 26 1030 38 3,080,864 19 0N 0K LC 27 0700 37 3,127,579 19 0N 0K LC 28 0630 38 3,179,467 20 0N 0K LC 29 0700 37 3,233,857 18 0N 0K LC 29 0700 37 3,289,222 19 0N 0K LC	12	0721	42	2,322,560	25	40	ΛV	1.0
14	13	0700	42		24			
15	14	1600	4-0					
16 0700 38 2,558,340 21 0N 0K LC 17 18 19 0700 37 2,720,819 20 0N 0K LC 20 0830 39 2,777,245 19 0N 0K LC 21 0900 37 2,836,456 20 0N 0K LC 22 0700 37 2,853,596 19 0N 0K LC 23 1030 38 2,918,821 18 0N 0K LC 24 25 26 1030 38 3,080,864 19 0N 0K LC 27 0700 37 3,127,579 19 0N 0K LC 28 0630 38 3,179,467 20 0N 0K LC 29 0700 37 3,233,857 18 0N 0K LC 30 0800 37 3,289,222 19 0N 0K LC	15	0600	41					
17 18 19	16	0700	38					
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20 0830 39 2,777,245 19 0N 0K LC 21 0900 37 2,836,456 20 0N 0K LC 22 0700 37 2,858,596 19 0N 0K LC 23 1030 38 2,918,821 18 0N 0K LC 24 25 26 1030 38 3,080,864 19 0N 0K LC 27 0700 37 3,127,579 19 0N 0K LC 28 0630 38 3,179,467 20 0N 0K LC 29 6700 37 3,233,857 18 0N 0K LC 30 0800 37 3,289,222 19 0N 0K LC	18				я			
20 0830 39 2,777,245 19 0N 61K LC 21 0900 37 2,836,456 20 0N 61K LC 22 0700 37 2,858,596 19 0N 6K LC 23 1030 38 2,918,821 18 0N 6K LC 24 25 26 1030 38 3,080,864 19 0N 6K LC 27 0700 37 3,127,579 19 0N 6K LC 28 0630 38 3,179,467 20 0N 6K LC 29 0700 37 3,233,857 18 6N 6K LC 30 0800 37 3,289,222 19 0N 6K LC	19	0700	37	2,720,819	20	00	OV	1.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20	0830	39		19			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	21	0900	37					
23	22	0700	37					
24	23	1030	38					
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27 0700 37 3,127,579 19 0N 0K LC 28 0630 38 3,179,467 20 0N 0K LC 29 0700 37 3,233,857 18 0N 0K LC 30 0800 37 3,289,222 19 0N 0K LC	25							
27 0700 37 3,127,579 19 0N 0K LC 28 0630 38 3,179,467 20 0N 0K LC 29 6700 37 3,233,857 18 6N 0K LC 30 0800 37 3,289,222 19 0N 0K LC	26	1030	38	3,080,864	19	60	OK	1.0
28 0630 38 3,179,467 20 ON OK LC 29 0700 37 3,233,857 18 ON OK LC 30 0800 37 3,289,222 19 ON OK LC	27	0700	37	7				
29 6760 37 3,233,857 18 ON OK LC 30 0800 37 3,289,222 19 ON OK LC	28	0630	38					
30 0800 37 3,289,222 19 ON OK LC	29	0700						
	30	0800	37					
	31			, , ,			0,5	

Day	Time	Flow Meter Reeding	Gations Discharged	Water Pressure (pal)	Air Stripper Blower On/Off	Air Stripper Condition	Inspector
1							
2	0813	37	3.449.110	18	60	6K	LC.
3	1526	36	3,515,690	16	00	ok	LC
4	1443	37	3,566,530	16	60	o.k.	La
5	0700	36	3,602,581	16	00	ok	ha
•	0940	37	3,660,390	18	0 <i>0</i>	OK	he
7							
8							
9	0718	36	3, 811, 680	18	60	OK	LC
10	1447	35	3,878,110	17	00	OK	٨
11	1440	35	3.928,610	15	0.1	ok	LC
12	1407	28	3.975990	7	60	OK	Le
13	0700	28	4,003,949	7	00	ok	40
14							
15							
18	1017	28	4,108,190	7	60	OK	rc
17	1030	23	4,142,336	7	00	O K.	LC.
18	0720	23	4,170,030	7	60	ok	LC
19	0730	34	4,221 505	12	00	OK	24
20	10:00	3.5	4, 277, 473	15	60	OK	24
21			, , , ,				
22							
23	11:35	36	4,440,580	16	60	OK	LC
	09:45	34	4,478,700	14	00	OK	LC
25	10:00	3.5	4,528,932	15	60	OL	LC
26	10:27	35	4.579690	15	0.0	o K	٨٥
27	15:38	34	4,640,320	1.5	60	OK	LC
28		<u> </u>					
29 30	0700	36	4,778,713	15	60	OK	4c
	2700	<u> </u>	-171101113			~~	

SENT

HUSSMANN SECO TREATMENT INSPECTION LOG

n Log Month and Year May 90 Daily Inst

18 OFF Flood 19 20 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 OFF Flood 27 OFF Flood 28 OFF Flood 29 OFF Flood 20 OFF Flood 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 OFF Flood 27 OFF Flood 28 OFF Flood 29 OFF Flood 20 OFF Flood 20 OFF Flood 20 OFF Flood 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 OFF Flood 27 OFF Flood 28 OFF Flood 29 OFF Flood 30 I3:45 32 Same As 5-17-80 IA Started System 13:45 on 5-30-90 wells 1, 2 & 3			T		T	7			
1 12.15 36 4,881,479 16 2 1348 36 4,885,010 15 0N OK LC 3 1200 35 4,931,896 15 0N OK AC 4 1030 35 4,931,896 16 0N OK AC 5 1045 34 5,124,589 13 0N OK AC 8 1100 33 5,172,750 13 ON OK AC 9 1205 32 5,224,673 12 ON OK AC 11 1400 31 5,325,933 12 ON OK AC 12 11 1400 31 5,325,933 12 ON OK AC 13 13 0N OK AC 14 1447 32 5,465,240 12 ON OK AC 15 1340 32 5,510,820 15 ON OK AC 16 1040 35 5,518,890 16 ON OK AC 17 0630 Noc Oberation 5,534,440 O System Down Due To Floating 18 OFF Flood 19 OFF Flood 19 OFF Flood 20 OFF Flood 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 OFF Flood 27 OFF Flood 28 OFF Flood 29 OFF Flood 30 13:45 3.2 Same Ps 5-17-90 14 Stanta System 13:45 on 5-30-90 20 OFF Flood 30 13:45 3.3 Same Ps 5-17-90 14 Stanta System 13:45 on 5-30-90 20 OFF Flood 30 13:45 3.3 Same Ps 5-17-90 14 Stanta System 13:45 on 5-30-90 20 OFF Flood 30 13:45 3.3 Same Ps 5-17-90 16 ON OK AC 20 ON KE SILE 20 OFF Flood 31 13:45 3.3 Same Ps 5-17-90 16 ON OK AC 21 OFF Flood 32 OFF Flood 33 13:45 3.3 Same Ps 5-17-90 16 ON OK AC 22 OFF Flood 34 OFF Stood 35 OFF Stood 36 OFF Stood 37 OFF Stood 38 OFF Stood 39 OFF Stood 30 OK AC 20 ON SAME DOWN IN STORY IN ST	Day	Time	Reading	Gallons Discharged		Air Stripper Blower On/Off	Air Stripper Condition	Inspector	
3 1200 35 4,93,896 15 00 0K 60 4 1030 35 4,978,066 16 0N 0K 60 5 6 7 1045 34 5,124,589 13 0N 0K 60 8 1100 33 5,172,750 13 0N 0K 60 12 130 32 5,274,173 12 0N 0K 60 11 1400 31 5,325,933 12 0N 0K 60 12 13	1	1215		4,821,479	16				1
3 1200 35 4,931896 15 ON OK AC 4 1030 35 4,973,066 16 ON OK AC 5 100 35 4,973,066 16 ON OK AC 6 1100 33 5,172,750 13 ON OK AC 9 1205 32 5,224,173 12 ON OK AC 10 1230 32 5,274,190 12 ON OK AC 11 1400 31 5,325,933 12 ON OK AC 12 13 ON OK AC 15 1340 32 5,510,820 15 ON OK AC 16 1040 35 5,518,890 16 ON OK AC 17 0630 Not Opening 5,534,440 O System Down Dire to Flooding Tomer English with System West OFF 15 OUT OF Flood 18 OFF Flood 20 OFF Flood 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 OFF Flood 27 OFF Flood 28 OFF Flood 29 OFF Flood 20 OFF Flood 20 OFF Flood 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 OFF Flood 27 OFF Flood 28 OFF Flood 29 OFF Flood 30 33:45 32 Samp Rs 5-17-70 14 Started Sizerm 13:45 on 5-30-70 Walls 1,243	2	1348	36	4,885,010	15	02	OK	LC	-
4 1030 35 4,978,066 16 0N 0K KC 5	3	1200		4,931,896	15	40			1
5	4	1030	35		16		OK		1
7 1045 34 5,124,589 13 0N OK NC 8 1100 33 5,172,750 13 ON OK NC 9 1205 32 5,224,(73 12 ON OK NC 10 1230 32 5,274,170 12 ON OK NC 11 1400 31 5,325,933 12 ON OK NC 12 0N OK NC 13 ON OK NC 14 14:47 32 5,465,240 12 ON OK NC 15 1340 32 5,510,820 15 ON OK NC 16 1040 35 5,518,890 16 ON OK NC 17 0630 Not Oberia, 5,534,440 O System Down Due To Flording 18 OFF Flood 20 OFF Flood 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 OFF Flood 27 ON OFF Flood 28 OFF Flood 29 OFF Flood 20 OFF Flood 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 OFF Flood 27 ON OK NC 28 OFF Flood 29 OFF Flood 30 OFF Flood 31 O745 33 5572780 16 ON OK NC 31 O745 33 5572780 16 ON OK NC 32 OFF Flood 33 O745 33 5572780 16 ON OK NC 34 OFF Flood 35 OFF Flood 36 OFF Flood 37 ON OK NC 38 OFF Flood 39 OFF Flood 30 OFF Flood 30 OFF Flood 30 OFF Flood 31 O745 33 5572780 16 ON OK NC 30 ON OK NC 31 ON OK NC 32 OFF Flood 33 OFF Flood 34 OFF Flood 35 OFF Flood 36 OFF Flood 37 ON OK NC 38 OFF Flood 39 OFF Flood 30 ON OK NC	5								-1
8 1100 33 5,172,750 13 ON OK AC 9 1205 32 5,224,673 12 ON OK AC 10 1230 32 5,274,190 12 ON OK AC 11 1400 31 5,325,933 12 ON OK AC 12	6								1
8 100 33 5,172,750 13 ON OR AC 9 1205 32 5,224,673 12 ON OR AC 10 1230 32 5,274,90 12 ON OR AC 11 1400 31 5,325,933 12 ON OR AC 12 ON OR AC 13 ON OR AC 14 14,47 32 5,465,240 12 ON OR AC 15 1340 32 5,510,820 15 ON OR AC 16 1040 35 5,518,890 16 ON OR AC 17 0630 Not Obering 5,534,440 O System Down Due to Floring OFF 15 UNKnown 18 OFF Flood 19 ON OR AC THE SWEET OFF 15 UNKnown 20 OFF Flood 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 OFF Flood 27 OFF Flood 28 OFF Flood 30 OFF Flood 31 32,557780 14 Started Sixtem 13:45 on 5-30-90 30 13:45 32 Same As 5-17-90 14 Started Sixtem 13:45 on 5-30-90 31 13:45 32 Same As 5-17-90 16 ON OR AC Week Unider 31 OFF Flood 31 13:45 33 S572780 16 ON OR AC Week Unider 32 OFF Flood 33 13:45 33 S572780 16 ON OR AC Week Unider	7	1		5, 124, 589	13	00	0 IC	LC	1
1205 32 5,224,673 12 0N 0K KC 10 1230 32 5,274,190 12 0N 0K KC 11 1400 31 5,325,933 12 0N 0K KC 12 13 14 14.47 32 5,465,240 12 0N 0K KC 15 1340 32 5,510,820 15 0N 0K KC 16 1040 35 5,518,890 16 0N 0K KC 17 0630 Not OPENING 5,534,440 0 System Down Due To Flooding Time System were off to OFF Tood 19 0N 5-16,-90 20 0FF Flood 0N 0N 0N 0N 21 0FF Flood 0N 0N 0N 0N 22 0FF Flood 0N 0N 0N 0N 23 0FF Flood 0N 0N 0N 24 0FF Flood 0N 0N 0N 25 0FF Flood 0N 0N 0N 0N 26 0N 5-17-90 N 27 0N 5-17-90 N 28 0FF Flood 0N 0N 0N 0N 0N 29 0FF Flood 0N 0N 0N 0N 0N 20 0N 5-17-90 N 21 0N 5-17-90 N 22 0N Flood 0N 0N 0N 0N 0N 24 0N 5-17-90 N 25 0N Flood 0N 0N 0N 0N 0N 0N 0N 26 0N 5-17-90 N 27 0N 5-17-90 N 28 0FF Flood 0N 0N 0N 0N 0N 0N 29 0N 5-17-90 N 20 0N 5-17-90 N 21 0N 5-17-90 N 22 0N 5-17-90 N 23 0N 5-17-90 N 24 0N 5-17-90 N 25 0N 5-17-90 N 26 0N 5-17-90 N 27 0N 5-17-90 N 28 0N F Flood 0N 0N 29 0N 5-17-90 N 20 0N 5-17-90 N 20 0N 5-17-90 N 21 0N 5-17-90 N 22 0N 5-17-90 N 23 0N 5-17-90 N 24 0N 5-17-90 N 25 0N 5-17-90 N 26 0N 5-17-90 N 27 0N 5-17-90 N 28 0N 5-17-90 N 29 0N 5-17-90 N 20 0N 5-17-90 N 20 0N 5-17-90 N 21 0N 5-17-90 N 22 0N 5-17-90 N 23 0N 5-17-90 N 24 0N 5-17-90 N 25 0N 5-17-90 N 26 0N 5-17-90 N 27 0N 5-17-90 N 28 0N 5-17-90 N 29 0N 5-17-90 N 20 0N 5-17-90 N 20 0N 5-17-90 N 21 0N 5-17-90 N	8	1100	33		13	00	OK	LC	1
10 1230 32 5,274,90 12 ON OK AC 11 1400 31 5,325,933 12 ON OK AC 12 ON OK AC 13 ON OK AC 14 14.47 32 5,465240 12 ON OK AC 15 1340 32 5,510,820 15 ON OK AC 16 1040 35 3,518,890 16 ON OK AC 17 0630 Not OPENING 5,534,440 O System Down Due To Flading OFF 150 UNKNOWN 18 OFF Flood 20 OFF Flood 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 OFF Flood 27 OFF Flood 28 OFF Flood 29 OFF Flood 30 13:45 32 Same fts 5-17-70 14 Stavet System 13:45 on 5-30-90 Wells 1,2 f 3 31 0745 33 5572780 16 ON OK AC Were Onder	9	1205		5, 224, 673	12	02	OK	40	1
12 13 14 14:47 32 5,465240 12 0N 0K AC 15 1340 32 5,510,820 15 0N 0K AC 16 1040 35 5,518,870 16 0N 0K AC 17 0630 Not OPEnairy 5,534,440 0 System Down Due To Flooding 18 0FF Flood 19 20 21 0FF Flood 22 0FF Flood 23 0FF Flood 24 0FF Flood 25 0FF Flood 26 27 28 0FF Flood 28 0FF Flood 29 0FF Flood 20 20 21 0FF Flood 22 0FF Flood 23 0FF Flood 24 0FF Flood 25 0FF Flood 26 27 28 0FF Flood 30 13:45 32 5ame As 5-17-80 14 5ba-bet System 13:45 on 5-30-90 00-15, 12 discontinuation of Area 0630 Inspection 07 The Site 18 19 10 10 10 10 10 10 10 10 10 10 10 10 10	10	1		.,	12	40	ok		1
12 13 14 14:47 32 5,465,240 12 0N 0K AC 15 1340 32 5,510,820 15 0N 0K AC 16 1040 35 5,518,890 16 0N 0K AC 17 0630 Not OPERATING SYSTEM DOWN DUR TO Flooding 18 0FF Flood 19 0N 5-16-90 20 20 21 0FF Flood 22 0FF Flood 23 0FF Flood 24 0FF Flood 25 0FF Flood 26 27 28 0FF Flood 30 13:45 32 5-18 \$ 5-17-90 15 0N 0N 0K AC 0FF DUC TO SYSTEM WENT TIME SYSTEM WENT OFF IS O'D KNOW THE SYSTEM WENT THE SYSTEM WENT TO FIND SYSTEM WENT THE SYSTEM WENT TO FIND SYSTEM TO FIND	11	1400	31	5,325,933	12	40	OK	LC	1
14 14.47 32 5,465,240 12 ON OK AC 15 1340 32 5,510,820 15 ON OK AC 16 1040 35 5,518,890 16 ON OK AC 17 0630 Not OPEnating 5,534,440 O System Down Due To Flooding 18 OFF Flood 20 At 1745 System 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 OFF Flood 27 OFF Flood 28 OFF Flood 29 OFF Flood 20 OFF Flood 20 OFF Flood 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 OFF Flood 27 OFF Flood 28 OFF Flood 29 OFF Flood 30 13:45 32 Same fts 5-17-90 14 Stavet System 13:45 on 5-30-90 wells 1,2 f 3 31 0745 33 5572780 16 ON OK AC Were Older	12		 						1
15 1340 32 5,510,820 15 0N OK NC OFF DUCTO Secon-SY. 16 1040 35 5,518,890 16 ON OK NC OFF DUCTO Secon-SY. 17 0630 Not OPENING 5,534,440 O SYSTEM DOWN Due TO Flooding Touries Back ON OFF 15 UNKNOWN. 18 OFF Flood 20 CH Flood 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 ON OFF Flood 27 CH COMMANDER OFF COM	13								1
15 1340 32 5,510,820 15 ON OK RC OFF DUE TO SECURD SET 17 OG 30 Not OPERATING 5,534,440 O SYSTEM DOWN DUE TO Flood OFF IS UNKNOWN OFF IS UNKN	14	1	32	5,465,240		010	O IC	LC	· ·
16 1040 35 5,518,890 16 ON OK AC OFF DUCTO Steven-Sy. 17 0630 Not OPE-asing 5,534,440 O System Down Due To Flooding Time System wenter 18 OFF Flood 19 005-16-90 20 005-16-90 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 0065-17-90 Ac 27 0630 Nospection 28 OFF Flood 29 OFF Flood 20 0630 Nospection 20 0630 Nospection 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 OFF Flood 27 OCCOMPANY 28 OFF Flood 29 OFF Flood 30 13:45 32 Same As 5-17-80 14 Stavet 2 System 13:45 ov 5-30-90 Wells 1, 2 \(\frac{1}{3} \) 31 0745 33 5572780 16 ON OK AC Were Under	15	1			15		OK	hc	5-15 \$ 5-16-90
18 OFF Flood 20	16	1	1		16	60		LC OFF	Due To Storm- Syst
19 20 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 OFF Flood 27 28 OFF Flood 28 OFF Flood 29 OFF Flood 30 13:45 32 Same As 5-17-70 14 Started Signer 13:45 on 5-30-90 wells 1, 2 \(\frac{2}{3}\) 31 0745 33 5572780 16 OD OK LC were under	17	 		5,534,440	0	System Down	Due To Flow	dive	Time System Went
20 21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 27 28 OFF Flood 29 OFF Flood 30 13:45 32 Same As 5-17-70 14 Stavled System 13:45 on 5-30-90 Wells 1, 2 & 3 3 1 0745 33 5572780 16 On OK RC Were Under	18	OFF	Frood	-				3	
21 OFF Flood 22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 OFF Flood 27 OFF Flood 28 OFF Flood 29 OFF Flood 30 13:45 32 Same As 5-17-90 14 Staved System 13:45 on 5-30-90 Wells 1, 2 \(\frac{2}{3} \) were under	19								00 5-16-90
22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 OFF Flood 27 OBS Shull Down Because Potentie For Overlight Flooding of Area Was Likely -4 OBS -17-90 At OBS OBS -17-90 At OBS OBS OBSPECTION OF The Site Revealed Tha 30 13:45 32 Same As 5-17-70 14 Started System 13:45 on 5-30-90 Wells 1, 2 & 3 11 0745 33 5572780 16 OD OK LC Were Obder	20								At 1745 Systa
22 OFF Flood 23 OFF Flood 24 OFF Flood 25 OFF Flood 26 27 28 OFF Flood 29 OFF Flood 20 OFF Flood 20 OFF Flood 21 22 23 OFF Washing of Area 24	21	 							Was Shut Down
23 OFF Flood 24 OFF Flood 25 OFF Flood 26	22	OFF							Because Potential
24 OFF Flood 25 OFF Flood 26 27 28 27 28 29 OFF Flood 29 OFF Flood 30 13:45 32 Same As 5-17-90 14 Started System 13:45 on 5-30-90 Wells 1, 2 \(\frac{2}{3}\) 31 0745 33 5572780 16 ON OK LC Were Under	23	1	Flood		***************************************				•
28 OFF Flood 29 OFF Flood 30 13:45 32 Same As 5-17-90 14 Started System 13:45 on 5-30-90 wells 1, 2 \(\frac{1}{2}\) 31 0745 33 5572780 16 ON OK LC were Under	24		Flood						Flooding of Area
28 OFF Flood 29 OFF Flood 30 13:45 32 Same As 5-17-90 14 Started System 13:45 on 5-30-90 wells 1, 2 \(\frac{1}{2}\) 31 0745 33 5572780 16 ON OK LC were Under	25	OFF	Flood						was Likely - Le
27 28 OFF Flood 29 OFF Flood 30 13:45 32 Same As 5-17-90 14 Started System 13:45 od 5-30-90 wells 1, 2 \(\frac{2}{3}\) 31 0745 33 5572780 16 OD OK LC were Under	26								
28 OFF Flood 29 OFF Flood 30 13:45 32 Same As 5-17-90 14 Started System 13:45 of 5-30-90 wells 1, 2 \(\frac{2}{3}\) 31 0745 33 5572780 16 ON OK LC were Under	27								
30 13:45 32 Same As 5-17-90 14 Started System 13:45 of 5-30-90 Wells 1, 2 & 3 31 0745 33 5572780 16 OD OK LC Were UDder	28	OFF							
31 0745 33 5572780 16 ON OK LC Were UNder	29								Revealed That
				Same As 5-17-90	14	Started SKS	tem 13:45 ou	5-30-90	wells 1, 2 & 3
	31	0745	33	5572780	16	00	OK	LC	

05-17-90 AE 630 INSPECTION The Site executed That ells 1,2 &3 iere unger water - system Remained off F

3142397859+

N

15128837565;#

; 6-29-90 8:32AM;

SENT BY: SECO

Day	Time	Flow Meter Reading	Gallons Discharged	Water Pressure (pel)	Air Stripper Blower On/Off	Air Stripper Condition	Inspector	
1	1330	34	5632880	20	00	ox	Lc	
2		. O+	er Meekend					
3	Due To	Storm A	Power Was of	+ Mowday 6-	3-70 - Tuyne	e System on	@ 0845 (he)	Erach Time S
4	0845	34	5,762490	19	0NE0845	OK	LC	west of U
5	0900	32	5810660	15	60	ok	LC .	
6	1545	29	5868490	12 ,	00	οk	LC	
7	1200	28	5,899,903	12	00	6 K	La	
8	1530	37	5915650	19	an	OK	LC	RW11 Stant
9			,	Ý				@ APP-0 x. 140
10								6-8-90 SY
11	1415	34	6,064,540	15	07	OK	Le	Dows os 6
12	6750	34	6,101,060	17	00	0 K	Le	Exact Ame
13	1437	33	6,164,030	14	00	OK	45	of Dows -
14	1525	32	6,213,908	12	69	o K-	he	UNKNOWN
15	1447	32	6,258,710	12	00	OK	LC	
16			'					
17								
16	1630	32	6,397,768	12	00	OK	LC	
19	1605	32	6,442,850	12	00	OK	LC	
20	0950	32	6,475,890	_15	60	OK	LC	
21	0955	30	6,520,185	15	60	o K	لرر	
22	1000	30	6, 563, 255	15	60	OK	LC	
23			,					
24								
25	0850	28	6,690,460	14	00	OK	LC	
28	0830	28.	6.730,930	13	60	ok	LC	
27	0930	28	6,773,350	13	40	OK	٢٧	
28	0950	29	6,815,544	12 .	0 N	OK	Le	
29	0815	29	6,855240	12	00	ok	rc	
30								
31								

							
Day	Time	Flow Meter Reading	Gallons Discharged	Water Pressure (psl)	Air Stripper Blower On/Off	Air Stripper Condition	Inspector
1							
2	0815	34	6,979,997	20	60	OK	Le
3	0830	35	7,030,704	21	40	ok	LC
4	Hoilda	Y					
5	0915	35	7,107,715	20.	00	OK	GB
6	0825	34	7,156,532	20	OD	01-	Gß
7							
8							
9	1433	34	7, 313,580	20	0N	014	GB
10	0837	30	7,349,170	18	00	OK	LC
11	0750	32	7,394,036	18	00	0 K	Le
12	0745	32	7,439,910	17	40	OK	Le
13	0730	32	7,485,396	18	60	٥١	Le
14							
15							
16	0750	32	7,620,415	21	02	OK	LC.
17	1530	28	7,678,060	19	00	OK	LC "
18	1200	32	7,718,220	20	00	. O IC-	Le
19	1200	33	7,765,020	20	00	010	he
20	0900	33	7,806,390	20	02	OK	LC
21			,	×			
22							
23	0950	33	7,948,380	22	60	O.K	LS
24	0900	33	7,993,850	21	00	01:	LC
25	1030	34	8,043580	22	40	0 K_	40
26	1030	32	8,092,050	22	00	010	LC
27	1100	34	8,137,620	21	40	OK	40
28			7 /				
29							
30	1130	33	8,279,700	22	00)	OR	40
31	1230	32	8,328,690	21	01	OK:	LC

1.000

4 1990

Day	Time	Flow Meter Reading	Gallons Discharged	Water Pressure (psl)	Air Stripper Blower On/Off	Air Stripper Condition	Inspector
1							
2							
3							
4							
5							
6							
7							
8							
9							
10						THE RESERVE OF THE PARTY OF THE	
11							
12							
13		ļ					
14	-	ļ					
15				-			
16	-						
17							
18							
19	1600	34	9,144,770	15	60	016	LC
20	1430	3.5	9,190,950	15	60	οĸ	LC
21	1630	34	9,244,160	15	60	0 15	LC
22							
23							
24	1630	34	9,390,590	16	00	OK	LC
25	1500	36	9,439,180	16	60	OK	ha
26	1400	35.	9,490,340	16	60	OK	LC
27	1530	36	9,543,780	20	00	016	La
28	1200	36	9,587,890	16	40	OK	LC
29							
30							
31							

9-19-90 System Started UP-Tower Completely Cleanet out -

TREATMENT ' 'T INSPECTION LOG

on Log Month and Year Oct. 90

-	7	7	7				7
Day	Time	Flow Meter Reading	Gallons Discharged	Water Pressure (psl)	Air Stripper Blower On/Off	Air Stripper Condition	Inspector
1	1600	35	9,751,750	15	OB	OK	hc
2	1400	3.5	9,798,220	15	40	OK	Lc
3	1630	34	9,853,870	15	60	IOK	L C
4	1430	3.5	9,899,090	16	00	OK	he
5	1200	3.5	9,943,180	1.5	02	OIC	LC
6							
7							
8	1500	36	10,106,220	19	2	015	he
9	1700	3.7	10, 165, 030	20	60	OK	ne
10	1630	37	10,223,550	21	02	010	h 9
11	1430	36	10,271,270	16	ao	OK	L C
12	1100	35	10,315,760	20	99	OK	LC
13			,				
14							
15	0900	38	10, 467, 890	20	60	014	hc
16	0800	39	10,517,380	20	60	010	Lc
17	0900	39	10,571,770	19	010	0 K	LC
18	1500	39	10,590,010	18	00	. 010	LC
19	1600	38	10,645,290	17	40	014	LC
20			,				
21							
22	1000	38	10,790,840	20	02	O IC	hC.
23	0830	36	10,837,320	19	00	OK	LC LC
24	1500	37	10,905,990	16	00	OK	LC
25	1200	38	10,948,900	17	ao	OIC	LC
26	1000	38.	10,999,430	18	60	OK	LC LC
27							
28							
29	0730	3 6	11, 147, 460	16	60	0/C	LC
30	900	35	11,201740	16	40	OK	LC
31	1200	37	11,263,640	18	00	OK	Le

1400 HVS.ON
10-18-90 FOUND
SYSTEM Shut
DOWN- Belier
It was Causal
By Storm ON
EVEN: 140 of
10-17-90- Turk
ed System ON
Q1410 of Let
RUN- Took
Readings @
1500 HVS-

TREATMENT ''NIT INSPECTION LOG RECEIVED DEC 0 7 1990

Dally In: on Log Month and Year Nov. 90

6	1	Flow Meter	Called			T	7
Day	Time	Reading	Gallons Discharged	Water Pressure (psl)	Air Stripper Blower On/Off	Air Stripper Condition	Inspector
1	1100	36	11, 315, 880	18	40	o K	La
2	1030	37	11, 366,420	19	00	OK	Lc
3						{	
4	ļ						
5	1200	36	11,524,430	19	40	OK	hs
6	1330	37	11,579,700	20	40	OK	hs
7	0700	36	11,616,990	20	00	OK	LC
8	1530	36	11,686,890	20	60	OK	hc
9	1600	36	11,739,750	20	02	ok.	he
10							
11							
12	1400	35	11,888,140	15	40	OK	hc.
13	1200	35	11,934,910	15	OD	OK	hc
14	1430	36	11,991,640	15	60	010	Le
15	0730	36	12,028,170	20	00	0/6	LC
16	1430	35	12,093,980	17	60	014	LC.
17							
18							
19	0900	35	12,235,570	19	00	ok	LC
20	1100	35	12,290,540	19	01)	O IC	rc
21	0700	36	12, 333,590	20	40	OK	LC
22	Ho1: 60	Υ					
23	Holidas	/					
24							
25							
26	0930	28	12,606850	14	40	OR	he
27	0800		12,644,810	14	40	OK	Le
28	1030		12,688,290	13	ON	016	LC
29	1630	30	12,780,520	12	00	OK	Le
30							
31							

Day	Time	Flow Meter Reading	Gallone Olsoharged	Water Preseure (psl)	Air Stripper Blower On/Off	Air Stripper Candition	Inspector
1	Holid						
2	Holid						
3	0730		13,823,420	7	ON	IOK	LC
4	0800	11	13,838,850	8	91	ok	bs
5							
6							
7	0900	11	13,843,240	8	02	OK	Lo
8	1630	10	13,863,190	9	00	OK	24
9	0800	12	13,876,160	9	02	ok	ha
10	0700	13	13,889,330	٩	OB	OK	hs
11	1030	13	13,908,850	8	0 N	01	LC
12							
13							
14	0900	12	13,911,260	4	60	OK	he
15	0700	18	13,935,540	10	CN	0 K	LC
16	0700	18	13, 962, 260	10	90	0K	LC
17	1230	19	13,944,870	10	0.0	ok	LC
18	0630	19	14,014,300	٩	ಎಬ	oK	2
19	·						
20	·						
21	0700	16	14,086,070	10	40	٥١٥	HC.
2	0730	20	14,113, 140	10	00	OK	La
3	1600.	22	14, 165, 740		60	0k	<u> </u>
24	0730	25	14, 188, 390	10	Op	OK	٨٥
25	0800	25	14, 224,540	9	40	OK	Le
8							
7							
8							
9							
0							-
			1	I			

Systen: Sometime (Haliday-Reset W

0700 on 1-

System T. Sover wer Turner one

0700 on 1-14

APPENDIX D

MONITOR/RECOVERY WELL DATA FORMS - 1990

HUSSI N SECO MONITOR/RECUVERY WELL DATA

Event Date: 1/29/90 (STATIC WATER LEVELS)

Monitor Well	Time	TOC Elevation	Depth To Water (TOC)	Water Elevation	TD Elevation	Pump On/Off	STARTING Flow Meter Reading (gal)	STARTING Flow Rate (gpm)	Water Pressure (psl)
MW-1	0743	482.02	Dry						
MW-2	0730	492.43	24.26	468.17					
MW-3	0735	482.81	Dry						
MW-4	0740	481.83	22.03	459.80					
MW-5	0807	484.24	26.37	457.87					
MW-6	0843	493.37	27.16	466.21					
MS-1	D818	482.32	22.82	459.50					2
MS-2	0745	482.75	24.80	457.95					
MS-3	0850	492.75	28.55	464.20					
MS-5	0830	491.95	31.66	460.29					
MS-6	0840	492.15	25.84	466.31					
SS-1	0810	483.22	Dry						
SS-2	0827	483.88	Dry						
SS-3	0824	492.14	Dry						
MD-1	0805	482.62	23.20	459.42					
MD-2	0748	482.58	21.98	460.60					
RW-1	0814	479.82	21.76	458.06		off	D	7.0	0
RW-2	0800	479.14	21.31	457.83		off	0	12.0	0
RW-3	0752	478.91	16.82	462.09		off	O.	8.0	0
RW-4	0820	483.84		459.76		off	0	1.5	0
RW-5	0835	486.84		464.47		off	15863	1.0	0

Dubois Creek

0900 493.27 34.50 458.77

HUSSI N SECO MONITOR/RECUVERY WELL DATA

Event Date: 1/29/90

Monitor Well	Time	TOC Elevation	Depth To Water (TOC)	Water Elevation	TD Elevation	Pump On/Off	Flow Meter Reading (gal)	Flow Rate (gpm)	Water Pressure (psl)
MW-1	1641	482.02	Dry			Ī			
MW-2	1630	492.43	24.31						
MW-3	1635	482.81	Dry						
MW-4	1639	481.83	22.45						
MW-5	1652	484.24	27.05						
MW-6	17/3	493.37	27.16						
MS-1	1658	482.32	23.79						
MS-2	1643	482.75	25.47						
MS-3	1717	492.75	28.59						
MS-5	1705	491.95	32.15						
MS-6	17/0	492.15	25.16						
SS-1	1654	483.22	Dry						
SS-2	1700	483.88	\mathcal{D}_{α}						
SS-3	1703	492.14	Dry						
MD-1	1650	482.62	23.10						
MD-2	1645	482.58	21.87						
RW-1	1534	479.82	29.83			DN		7. <i>0</i>	15
RW-2	1540	479.14	23.41			o N		12. U	10
RW-3	1545	478.91	41.50			ON		8.0	10
RW-4	1530	483.84	31.83			04		1.5	15
RW-5	1523	486.84	no meas. taken	4		off	_	0.0	15

1:

HUSSI N SECO MONITOR/REC-VERY WELL DATA

Event Date: //30/90

Monitor Well	Time	TOC Elevation	Depth To Water (TOC)	Water Elevation	TD Elevation	Pump On/Off	Flow Meter Reading (gal)	Flow Rate (gpm)	Water Pressure (psl)
MW-1	0745	482.02	Dry						
MW-2	0735	492.43	24.29						
MW-3	0738	482.81	Dry						
MW-4	0742	481.83	23.02						
MW-5	0758	484.24	27.20						
MW-6	0841	493.37	27.18						
MS-1	0819	482.32	24.35						
MS-2	0748	482.75	25.66					1	
MS-3	0845	492.75	28.50						
MS-5	0826	491.95	32.83						
MS-6	0839	492.15	25.72			***************************************			
SS-1	0800	483.22	Dry						
SS-2	0821	483.88	Dry						
SS-3	0823	492.14	Dry						
MD-1	0755	482.62	23.08						
MD-2	0750	482.58	21.85						
RW-1	0816	479.82	28.49			ON	6710	6.0/8.0	15
RW-2	0810	479.14	23.52			2N	2855	11.0/12.0	15
RW-3	0804	478.91	41.68			מא	8830	7.5/8.5	10
RW-4	0832	483.84	31.62			2 M	1420	1.25/1.5	15
RW-5	0837	486.84	34.34			off	15892	0.0	15

11

HUSS: 'N SECO MONITOR/RECOVERY WELL DATA

Event Date: 1/3//90

Monitor Well	Time	TOC Elevation	Depth To Water (TOC)	Water Elevation	TD Elevation	Pump On/Off	Flow Meter Reading (gal)	Flow Rate (gpm)	Water Pressure (psi)
MW-1	0745	482.02	Dry						
MW-2	0735	492.43	24.29						
MW-3	0740	482.81	Dry						
MW-4	0742	481.83	23.15						
MW-5	0802	484.24	27.04						
MW-6	0824	493.37	27.23	× .					
MS-1	0810	482.32	24.95						
MS-2	0750	482.75	25.50						
MS-3	0828	492.75	28.55						
MS-5	0815	491.95	32.48						
MS-6	0822	492.15	25.85						
SS-1	0804	483.22	Dry						
SS-2	0812	483.88	Dry						
SS-3	0814	492.14	Dry						
MD-1	0800	482.62	23.36						
MD-2	0752	482.58	22.15						
RW-1	0808	479.82	30.14			40	16235	7.0	
RW-2	0806	479.14	21.98			off	21063	0.0/20.0	
RW-3	0748	478.91	37.11			٥٨	19010	8.0/9.5	
RW-4	0817	483.84	25.03			off	1714	0.0/1.5	
RW-5	0820	486.84	35.72			off	15900	0.0	

reset any sousitive for all recovery well to Keep then from shutting off industrially.

Dubois Creek

0825 493.27

34.53

HUSS! 'N SECO MONITOR/REC-VERY WELL DATA

Event Date: 2/1/90

Monitor Well	Time	TOC Elevation	Depth To Water (TOC)	Water Elevation	TD Elevation	Pump On/Off	Flow Meter Reading (gal)	Flow Rate (gpm)	Water Pressure (psl)
MW-1	0812	482.02	Dry						
MW-2	0804	492.43	24.29				8		
MW-3	0807	482.81	Dry						
MW-4	0810	481.83	Dry						
MW-5	0822	484.24	27.80						
MW-6	0838	493.37	27.26						
MS-1	0824	482.32	24.86						
MS-2	0814	482.75	26.25						
MS-3	0840	492.75	28.38						
MS-5	0833	491.95	33.33						
MS-6	0836	492.15	25.79						
SS-1	0824	483.22	Dry						
SS-2	0828	483.88	Dry						
SS-3	0831	492.14	Dry						
MD-1	0820	482.62	23.18						
MD-2	0816	482.58	21.92						
RW-1	0902	479.82	30.91			04	26970	7.0	25
RW-2	09/0	479.14	25.07			DN	48450	19.5	20
RW-3	0916	478.91	40.64			04	33060	9.0/10.0	27
RW-4	0850	483.84	32.71			No	3324	1.5	23
RW-5	0845	486.84	33.84			off	15401	0.0	20

Dubois 0920 493.27 35.20

HUSS! 'N SECO MONITOR/RECUVERY WELL DATA

Event Date: 2/9/90

Monitor Well	Time	TOC Elevation	Depth To Water (TOC)	Water Elevation	TD Elevation	Pump On/Off	Flow Meter Reading (gal)	Flow Rate (gpm)	Water Pressure (psi)
MW-1		482.02	Dry						
MW-2		492.43	NO MEAS. Taked						
мw-з		482.81	Dry						
MW-4		481.83	22.70						
MW-5		484.24	28.00						
MW-6		493.37	27.30					Υ.	
MS-1		482.32	24.50						
MS-2		482.75	26.30						
MS-3		492.75	30.10						
MS-5		491.95	32.90						
MS-6		492.15	25,50						
SS-1		483.22	Dry						
SS-2		483.88	Dry						
SS-3		492.14	Dry						
MD-1		482.62	19.20						
MD-2		482.58	22.10						
RW-1		479.82	NO MESS. taken			OM	100230	7.10	20
RW-2		479.14	27.00			01	252572	20.80	25
RW-3		478.91	42.90			04	135607	10.60	30
RW-4		483.84	NO Meas. Laken			off	9421	D .0	25
RW-5		486.84	NO Mess. taken			off	15956	0.0	25

HUSS! IN SECO MONITOR/RECOVERY WELL DATA

Event Date: 2/22/90

Monitor Well	Time	TOC Elevation	Depth To Water (TOC)	Water Elevation	TD Elevation	Pump On/Off	Flow Meter Reading (gal)	Flow Rate (gpm)	Water Pressure (psi)
MW-1		482.02	Dry						
MW-2		492.43	NO MEAS. Taken						
MW-3		482.81	Dry						
MW-4		481.83	20.80						
MW-5		484.24	27.00						
MW-6		493.37	26.40						
MS-1		482.32	23.50						
MS-2		482.75	25.20						
MS-3		492.75	28.20						
MS-5		491.95	32.50						
MS-6		492.15	26.10						
SS-1		483.22	Dry						
SS-2		483.88	Dry		***************************************				
SS-3		492.14	Dry						
MD-1		482.62	23.10						
MD-2		482.58	22.30						
RW-1		479.82	24.20			04		7.0	
RW-2		479.14	24.50			04		18.0	
RW-3		478.91	42.20			04		10.0	
RW-4		483.84	25.00			off		0.0	
RW-5		486.84	31.70			off		0.0	

HUSSI N SECO MONITOR/RECOVERY WELL DATA

Event Date: 3/1/90

Monitor Well	Time	TOC Elevation	Depth To Water (TOC)	Water Elevation	TD Elevation	Pump On/Off	Flow Meter Reading (gal)	Flow Rate (gpm)	Water Pressure (psi)
MW-1		482.02	22.58						
MW-2		492.43	18.90						
MW-3		482.81	22.08						
MW-4		481.83	17.291						
MW-5		484.24	24.95						
MW-6		493.37	25.96						
MS-1		482.32	23.04						
MS-2		482.75	23.35						
MS-3		492.75	27.75						
MS-5		491.95	32.85						
MS-6		492.15	25.42						
SS-1		483.22	Dry			4	,		
SS-2		483.88	Dry						
SS-3		492.14	Dry						
MD-1		482.62	22.00						
MD-2		482.58	21.75						
RW-1		479.82	20.71			ON	163623	7.0/8.0	
RW-2		479.14	22.29			04	895778	18.0/22.0	
RW-3		478.91	34.83			01	452495	10.0/12.00	
RW-4		483.84	33.29			off	24900	-/1.5	
RW-5		486.84	33,21			off	16200	-/1.0	41 W - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1

FM cleaned

Dubois Creek

493.27

32.88

HUSS! IN SECO MONITOR/REC. JERY WELL DATA

Event Date: 3/2/90

Monitor Well	Time	TOC Elevation	Depth To Water (TOC)	Water Elevation	TD Elevation	Pump On/Off	Flow Meter Reading (gal)	Flow Rate (gpm)	Water Pressure (psi)
MW-1		482.02							
MW-2		492.43							
MW-3		482.81							
MW-4		481.83							
MW-5		484.24							
MW-6		493.37							
MS-1		482.32							
MS-2	and the second	482.75							
MS-3		492.75							
MS-5		491.95							
MS-6		492.15							
SS-1		483.22							
SS-2		483.88							
SS-3		492.14							
MD-1		482.62							
MD-2		482.58							
RW-1		479.82	24.24					8.0	
RW-2		479.14	22.29					22.0	
RW-3		478.91	42.44					12.0	
RW-4	MARKATER LANGE	483.84	37.21					1.5	
RW-5		486.84	35.62					1.0	

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HUSSMANN O MONITOR/RECOVERY WELL DATA

Event Date: 3/13/90

Monitor Well	Time	TOC Elevation	Depth To Water (TOC)	Water Elevation	TD Elevation	Pump On/Off	Flow Meter Reading (gal)	Flow Rate (gpm)	Water Pressure (psi)
MW-1	12:25	482.02	22.64'	459.38	-		3 (3-1)	india (gprii)	r ressure (psi)
MW-2	10:10	492.43	23.75'	468.68					
MW-3	10:20	482.81	22.06	460.75		1			
MW-4	10:30	481.83	17.79'	464.04			 		
MW-5	11:10	484.24	25.14	459.10					
MW-6	12:00	493.37	25.79'	467.58					
MS-1	11:30	482.32	23.90'	458.42					
VIS-2	12:20	482.75	23.54	459.21					
MS-3	16:30	492.75	28.17'	464.58					
MS-5	12:10	491.95	33.351	458.60			 		
MS-6	11:50	492.15	24.98'	467.17	***************************************				
SS-1	11:05	483.22	DRY						
SS-2	11:35	483.88	DRY			•	 		
SS-3	12:15	492.14	DRY						
1D-1	11:00	482.62	21.46	461.16					
ID-2	12:30	482.58		461.52					
W-1	11:20	479.82		451.56		ON	197200	FM HAD	2-
W-2	10:50	479.14		456.64		ON	1246240	STOPPED 20,5	25
W-3	10:40	478.91	001	135.99		0N	652460		
W-4	11:40	483.84		448,84		07	56730	11.6	30
W-5	11:45	486.84	,	451.03		off	16315	2 ¢	25 25

BRIDGE 16:40 493.27 31.88' 461.39 **2**002

C ? RINAMEZUH ATAC LLE. (PRIVODEN)ROTINOM

Event Cate:

Monitor Well	Time	TOC Elevation	Depth To Water (TOC)	Water Elevation	TD Elevation	Pump On/Off	Flow Meter Reading (gal)	Flow Rate (gpm)	Water Pressure (psl)
MW-1	1042	482.02	15.62						
MW-2	0920	492.43	22.52						
NIW-3	0-24	482.81	16.29					-	
NW-4	0928	481.83	13.77'						
MW-5	0948	484.24	20.04						
N W-6	1012	493.37	23.58						
N S-1	c957	482.32	18.40'						
N S-2	1239	482.75	18.77'						
N S-3	1016	492.75	25.83						
M-S-5	1004	491.95	23.29'						
M-S-6	1008	492.15	23.94'						
S3-1	c750	483.22	DRY						
S3-2	1000	483.88	WAY 18.5	(2')					
S3-3	1002	492.14	DRY						
MD-1	0943	482.62	18.60'						
MD-2	1037	482.58	18.75'						
R ™ V-1	0955	479.82	12.42'			OFF	197,201	Ø =	SYSTEM WILL
RTV-2	0740	479.14	17.81			ON	1,872,040	19.4	SYSTEM WILL CHECKED BURN WEEK OF
RYV-3	0933	478.91	36.58'			ON	1,004,800	13.5	
RW-4	1030	483.84	25. 85			ON	83780	0.8	
RW-5	1023	486.84	35.83			OFF	16520	Ø	

AR STRIPPER

BRIDGE

3,504,820

HUS NN SECO MONITOR/REWIVERY WELL DATA

Event Date: 4/12/90

Monitor Well	Time	TOC Elevation	Depth To Water (TOC)	Water Elevation	TD Elevation	Pump On/Off	Flow Meter Reading (gal)	Flow Rate (gpm)	Water Pressure (psi)
MW-1	10:42	482.02	15.75	(30UNDED)					
MW-2	10:50	492.43	22.51	(SOUNDED)					
MW-3	10:35	482.81	16.401	/ SOUNDED (@ 24.52')					
MW-4	10:38	481.83	13.67	(@24.62')					1
MW-5	10:26	484.24	20.59	(SOUNDED)					
MW-6	0947	493.37	24.17	(SOUNDED)				1	
MS-1	10:19	482.32	18.65'						
MS-2	10:40	482.75	19.23						
MS-3	0943	492.75	25.88'					<u> </u>	
MS-5	10:15	491.95	28.29'						
MS-6	0950	492.15	23.79'						
SS-1	10:24	483.22	DRY (7.10)						
SS-2	0940	483.88	18.85'	€ 22.45')					
S-3	10:17	492.14	DRY		~				
AD-1	10:28	482.62	18.77						
AD-2	10:44	482.58	18.83'						
W-1	10:21	479.82	12.39'			OFF	197201	ø	
IW-2	[0:30	479.14	18.25'			ON	2101050	4->	FLOWHETER FI CLOGGED => NO
W-3	10:33	478.91	37.46'			ON	1153410	11.5	CLOGGED
W-4	10:10	483.84	23.54			ON	103310	0.7	
W-5	10:00	486.84	35.71'			OFF	165597	ø	
RIDGE	0955		29,52'						

©3145693925 10:12 04/16/90

SUITES SERVICES

HUSSMANN SECT MONITOR/RECOVERY WE... DATA

rent Date: JULY 18,1990

Monitor Well	Time	TOC Elevation	Depth To Water (TOC)	Water Elevation	TD Elevation	Pump On/Off	Flow Meter Reading (gal)	Flow Rate (gpm)	Water Pressure (psi)
MW-1	11:23	482.02	13.26	468.76	· · · · · ·				
MW-2	10:00	492.43	18.28'	474.15					
WW-3	10:10	482.81	12.96	469.85					
WW-4	10:15	481.83	11.28'	470.55					
VW-5	10:55	484.24	19.85	464.39					
WW-6	11:35	493.37	22.56	470.81					
VIS-1	11:27	482.32	18.23		,				
VIS-2	11:15	482.75	18.541	464.21					
VIS-3	11:40	492.75	24.11	468.64					
VIS -5	12:05	491.95	27.68'	464.27					
45-6	11:50	492.15	41	471.50					,
i S-1	11:00	483.22		466.85					
iS-2	12:10	483.88	17.48'	466.40					
iS-3	11:30	492.14	20,31	471.83					
/ID-1	10:50	482.62	15.19	467.43					
1D-2	11:20	482.58	13.93'	468.65					
tW-1	11:05	479.82	20.77	457.12		ON	200722	FM STUCK	,
IW-2	10:35	479.14		461.75		OFF		No FM;	EPLACED
1W-3	10:20	478.91	, 1	454.91		ON	2110473	\$; FM STUC	2 1000H 25-00
W-4	12:00	483.84	. 71	449.00		ON	238214	3GPM	
₩-5	11:52	486.84	34,25			off	24414	φ	

21DGE 11:45 413.27 2 STRIPPER 12:15 31.05 462.22

7715420 30 GPM 7715420 30 GPM

HUSSMANN SECO MONITOR/RECO Y WELL DATA

BY STEDE WES

Event Date: 8-6-90

Monitor Well	Time	TOC Elevation	Depth To (Ci) Water (TOC)	Water Elevation	TD Elevation	Pump On/Off	Flow Meter Reading (gal)	Flow Rate (gpm)	Water Pressure (psi)
MW-1	1516	482.02	14.45						
MW-2	1525	492.43	19.10						
MW-3	1253	482.81	14.78						
MW-4	1230	481.83	13,42						
MW-5	1545	484.24	19.60	-					
MW-6	1635	493.37	33,55			,			
MS-1	1615	482.32	12,95						
MS-2	1510	482.75	1805						
MS-3	1646	492.75	35.03						
MS-5	1627	491.95	27.52						
MS-6	1631	492.15	92.00						
SS-1	1549	483.22	17,45						
SS-2	1610	483.88	19.95						
SS-3	1125	492.14	20.55						
MD-1	1543	482.62	15,80						
MD-2	1514	482.58	12.02						
RW-1	1553	479.82	22,40				0,222,599	Flow meter abot Sp NA	ming
RW-2	1559	479.14	17,40				0,172,710	23	***************************************
RW-3	1603	478.91	26,20				2,250,210	5.5	
RW-4	1619	483.84	30.82				0,300,091	2,5	
RW-5	1641	486.84	18.91				0.024.503	066	

HUSSMANN O MONITOR/RECOVER WELL DATA

Event Date: 10/10/90

Monitor Well	Time	TOC Elevation	Depth To Water (TOC)	Water Elevation	TD Elevation	Pump On/Off	Flow Meter Reading (gal)	Flow Rate (gpm)	Water Pressure (psi)
MW-1	1450	482.02	11.52.						
MW-2	1510	492.43	2135						
MW-3	1565	482.81	18'21						
MW-4	1500	481.83	14.18						
MW-5	1579	484.24	25.38						
MW-6	1555	493.37	24.26						
MS-1	1535	482.32	3218						
MS-2	1448	482.75	23.88						
MS-3	1600	492.75	2175						
MS-5	1548	491.95	31.78						
MS-6	1550	492.15	23.19						
SS-1	1525	483.22	17.56						
SS-2	1539	483.88	19.69						
SS-3	1544	492.14	22.03						
MD-1	1515	482.62	19:92						
MD-2	1445	482.58	18-48						
RW-1	1450	479.82	26.37	10/15/7	D	Ućf	0,122,554	088	
RW-2	1640	479.14	23.72			O_t	1,341,426	765	-
RW-3	1633	478.91	2367			O _C	2,515,462	61	
RW-4	1617	483.84	35:36			O _{c.}	0,394,170	2.1	
RW-5	1605	486.84	20.42			946	0.024,562	040	

AIR SCRIPFER

1700

10, 224,366 32,0